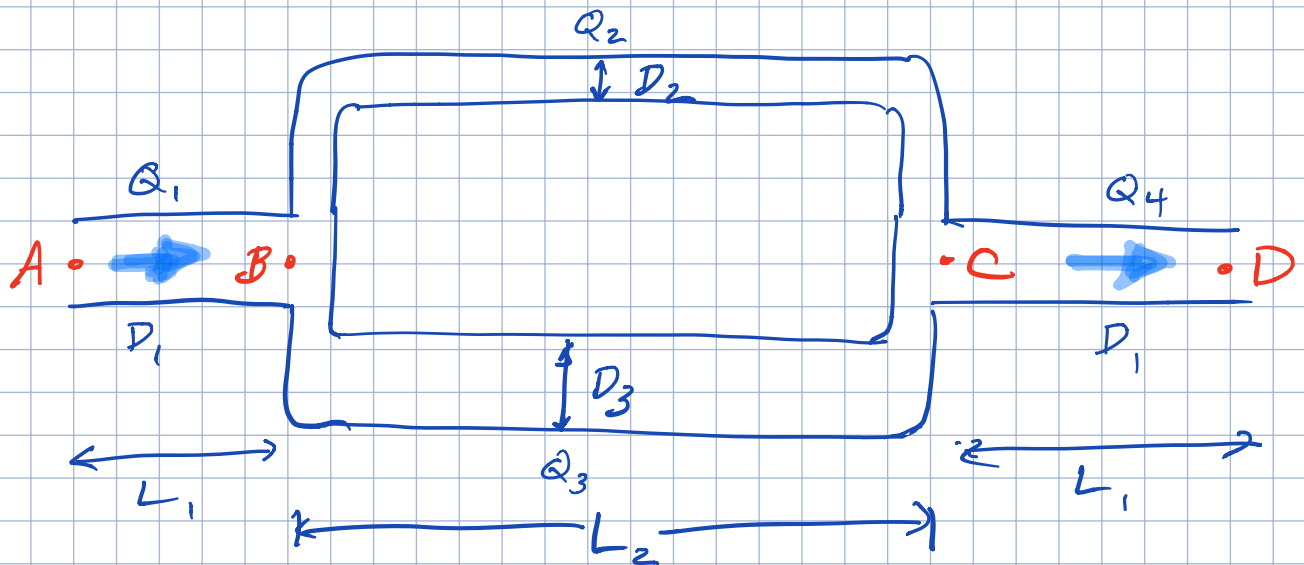


④



Re is low, neglect bends, splits

water: $\rho = 1000 \text{ kg/m}^3$ $\gamma = 0,001 \text{ Pa}\cdot\text{s}$

$$a) \quad Q_1 = Q_2 + Q_3 = Q_4$$

$$b) \quad \Delta P_{AB} = \Delta P_{CD} \quad \text{same } \langle v \rangle, \text{ same } D, \text{ same } l$$

$$\Delta P_{AD} = \Delta P_{AB} + \Delta P_{BC} + \Delta P_{CD}$$

$$\Delta P_{AD} = 2\Delta P_{AB} + \Delta P_{BC}$$

c) Since Re is low in all pipes, the flow rates & pressure drops are related by $f = \frac{16}{Re}$ or (equivalently) the Hagen - Poiseuille eqn:

$$Q = \frac{\pi}{128} \frac{\Delta P D^4}{L \gamma}$$

$$\text{so } Q_2 = \frac{\pi}{128} \frac{\Delta P_{BC} D_2^4}{L_2 \gamma}, \quad Q_3 = \frac{\pi}{128} \frac{\Delta P_{BC} D_3^4}{L_2 \gamma}$$

$$\Rightarrow \frac{Q_2}{Q_3} = \left(\frac{D_2}{D_3} \right)^4$$

From a)

$$Q_1 = Q_2 + Q_3 = Q_3 \left(1 + \left(\frac{D_2}{D_3} \right)^4 \right)$$

$$\Rightarrow \boxed{\frac{Q_3}{Q_1} = \frac{1}{\left(1 + \left(\frac{D_2}{D_3} \right)^4 \right)}} \quad (*)$$

d) From Hagen - Poiseuille eqn,

$$\Delta P_{BC} = \frac{128}{\pi} \eta \frac{L_2}{D_3^4} Q_3$$

$$\Delta P_{AB} = \frac{128}{\pi} \eta \frac{L_1}{D_1^4} Q_1$$

From part b)

$$\Delta P_{AD} = 2 \Delta P_{AB} + \Delta P_{BC}$$

$$\Rightarrow \Delta P_{AD} = \frac{128}{\pi} \eta \left[2 \frac{L_1}{D_1^4} Q_1 + \frac{L_2}{D_3^4} Q_3 \right]$$

$$\Delta P_{AD} = \frac{128}{\pi} \eta \left[2 \frac{L_1}{D_1^4} Q_1 + \frac{L_2}{D_3^4} Q_1 \frac{1}{\left(1 + \left(\frac{D_2}{D_3} \right)^4 \right)} \right]$$

$$\frac{\Delta P_{BC}}{\Delta P_{AD}} = \frac{\frac{L_2}{D_3^4} Q_1}{\left(1 + \left(\frac{D_2}{D_3} \right)^4 \right)}$$

$$= \frac{2 \frac{L_1}{D_1^4} Q_1 + \frac{L_2}{D_3^4} Q_1 \frac{1}{\left(1 + \left(\frac{D_2}{D_3} \right)^4 \right)}}{2 \frac{L_1}{D_1^4} + \frac{L_2}{D_3^4} \left(\frac{1}{1 + \left(\frac{D_2}{D_3} \right)^4} \right)}$$

$$= \frac{\frac{L_2}{D_3^4} \frac{1}{\left(1 + \left(\frac{D_2}{D_3} \right)^4 \right)}}{2 \frac{L_1}{D_1^4} + \frac{L_2}{D_3^4} \left(\frac{1}{1 + \left(\frac{D_2}{D_3} \right)^4} \right)}$$

$$= \frac{\frac{L_2}{D_3^4} \frac{1}{\left(1 + \left(\frac{D_2}{D_3} \right)^4 \right)}}{2 \frac{L_1}{D_1^4} + \frac{L_2}{D_3^4} \left(\frac{1}{1 + \left(\frac{D_2}{D_3} \right)^4} \right)}$$

$$\frac{\Delta P_{BC}}{\Delta P_{AD}} =$$

$$\frac{L_2/D_3^4}{2 \frac{L_1}{D_1^4} \left(1 + \left(\frac{D_2}{D_3} \right)^4 \right) + L_2/D_3^4}$$

$$= \frac{L_2/D_3^4}{2 \frac{L_1}{D_1^4} \left(1 + \left(\frac{D_2}{D_3} \right)^4 \right) + L_2/D_3^4}$$

$$e) \quad D_1 = 0.005 \text{ m}, \quad D_2 = 0.0021 \text{ m}, \quad D_3 = 0.003 \text{ m}$$

$$L_1 = 1 \text{ m}, \quad L_2 = 2.5 \text{ m}, \quad \Delta P_{AD} = 180 \text{ Pa}$$

$$\text{From } (*) \quad \frac{Q_3}{Q_1} = \frac{1}{1 + \left(\frac{D_2}{D_3}\right)^4} = 0.8064$$

$$\text{From } (**)$$

$$\frac{\Delta P_{BC}}{\Delta P_{AD}} = \frac{2.5 / (0.003)^4}{2 \left(\frac{1}{(0.005)^4} \left(1 + \left(\frac{0.0021}{0.003}\right)^4\right) + \frac{2.5}{(0.003)^4}\right)}$$

$$\Delta P_{BC} = 0.886 \Delta P_{AD}$$

$$= 0.886 (180 \text{ Pa}) = \underline{159.5 \text{ Pa}}$$

$$\Delta P_{AB} = \frac{1}{2} (\Delta P_{AD} - \Delta P_{BC}) \quad \text{from a)}$$

$$= \underline{10.25 \text{ Pa}}$$

$$Q_3 = \frac{\pi}{128 \eta} \frac{D_3^4}{L_2} \Delta P_{BC} = 1.268 \times 10^{-7} \frac{\text{m}^3}{\text{s}}$$

$$Q_1 = \frac{Q_3}{0.8064} = \underline{1.573 \times 10^{-7} \frac{\text{m}^3}{\text{s}}}$$

$$Q_2 = Q_1 - Q_3 = \underline{3.049 \times 10^{-8} \frac{\text{m}^3}{\text{s}}}$$

f) check Re

$$Re = \frac{\rho V D}{\eta}$$

$$Re_1 = \frac{\rho V_1 D_1}{\eta} = \frac{\rho}{\eta} \frac{Q_1}{\frac{\pi}{4} D_1^2} D_1 = \frac{4 \rho Q_1}{\pi \eta D_1} = \underline{40.06}$$

Since $Re_1 < 2100$ (or 4000), flow is laminar & eqns relating Q and Δp are appropriate. Assumption is ok.

g) No effect. Pipe roughness doesn't matter in laminar flow regime.

(a) Buckingham π analysis (7)

	<u>Variable</u>	<u>Dimensions</u>
0.5	Φ	$M L^2 T^{-3}$
0.5	D	L
0.5	u	$L T^{-1}$
0.5	ρ	$M L^{-3}$
0.5	η	$M L^{-1} T^{-1}$

5 variables - 3 independent dimensions (M, L, T)

\Rightarrow 2 dimensionless groups!

$D, u, \rho \rightarrow$ core variables.

+2 $\cdot N_1 = \frac{\Phi}{D^a u^b \rho^c} \Rightarrow$

$$\cong \frac{\Phi}{D^2 u^3 \rho}$$

$$M L^2 T^{-3} = M^c L^{a+b-3c} T^{-b}$$

$$\Rightarrow c=1, b=3, a=2$$

+1 $\cdot N_2 = \frac{D u \rho}{\eta} \equiv Re$ (as expected).

\Rightarrow General functional relation : $N_1 = f(N_2)$

+1.5 $\Rightarrow \boxed{\Phi = D^2 u^3 \rho f(Re)}$

(b) $\Phi \propto m^{3/4}$

But $m = \rho_f V \sim \rho_f D^3$

density of fish \uparrow Volume of fish.

assuming $V \sim D^3 \rightarrow +1$

$$\Rightarrow \Phi \sim \rho_f^{3/4} D^{9/4} = k \underbrace{\rho_f^{3/4}}_{C_0} D^{9/4} \quad (\text{Kleiber's law}) \quad +1$$

Thus all we need to assume is that the volume V scales as D^3

$$(c) \quad Re_m = \frac{0.5 \text{ m} \times 1 \text{ m/s} \times 1000 \text{ kg/m}^3}{10^{-3} \text{ Pa}\cdot\text{s}} = 5 \times 10^5 \gg 1 \quad +3$$

$$(d) \quad F_{D,m} = C_1 D_m^2 \rho U_m^2 \quad \rightarrow \text{Modern fish}$$

$$F_{D,G} = C_1 D_G^2 \rho U_G^2 \quad \rightarrow \text{Giant prehistoric relative.}$$

$$\Rightarrow \phi_m \propto F_{D,m} U_m \quad ; \quad \phi_G \propto F_{D,G} U_G$$

+3 +1

$$\Rightarrow \frac{\phi_G}{\phi_m} = \frac{F_{D,G} U_G}{F_{D,m} U_m} = \frac{C_0 D_G^{9/4}}{C_0 D_m^{9/4}} \quad (\text{from part c.})$$

$$\Rightarrow \frac{D_G^2 U_G^3}{D_m^2 U_m^3} = \frac{D_G^{9/4}}{D_m^{9/4}}$$

$$\Rightarrow \frac{U_G^3}{U_m^3} = \frac{D_G^{1/4}}{D_m^{1/4}}$$

$$\Rightarrow U_G = U_m \left(\frac{D_G}{D_m} \right)^{1/12} = 1 \text{ m/s} \times (10)^{1/12} \quad +2$$

$$\Rightarrow \boxed{U_G = 1.21 \text{ m/s}} \quad +1$$