

UNIVERSITY OF CALIFORNIA  
College of Engineering  
Department of Electrical Engineering  
and Computer Sciences

EE 42 / 100

Midterm 2

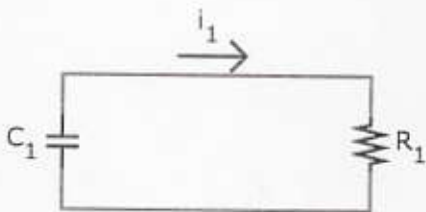
Spring 2008

Name: <i>Solutions</i>
SID:
Section:
Name of student left of you:
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Problem	Score
1	
2	
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Total	

- Check the units of your results.
- Closed book, closed notes.
- No calculators.
- Leave pack, books, and electronic devices (e.g. cell phones) in isle.
- Take off caps or hats.
- Copy your answers into marked boxes on exam sheets.
- Simplify numerical and algebraic results as much as possible.
- Be kind to the graders and write legibly. No credit for illegible results.
- No credit for multiple differing answers to the same question.
- The UC rules on dishonesty apply.

1. [25 points] A capacitor  $C_1$  is used to power a model airplane, represented in the circuit diagram below by resistor  $R_1$ . Initially the capacitor is charged to voltage  $V_1$ . Calculate the fraction  $r$  of the initial energy remaining on the capacitor when the current  $i_1$  has decreased to half its initial value.



$$r = \frac{1}{4}$$

The energy stored in a capacitor is given by

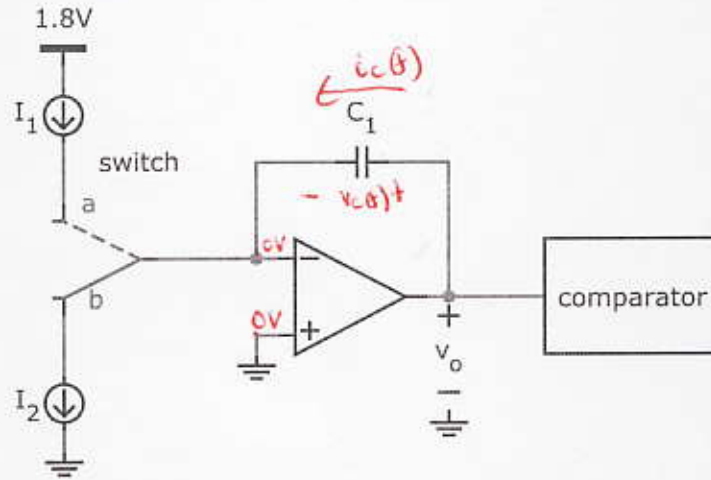
$$E_{\text{stored}} = \frac{1}{2} C V^2$$

$$E_0 = \frac{1}{2} C_1 V_0^2 = \frac{1}{2} C_1 V_1^2$$

$$E_f = \frac{1}{2} C_1 V_f^2 = \frac{1}{2} C_1 (I_f R_1)^2 = \frac{1}{2} C_1 \left(\frac{I_1 R_1}{2}\right)^2 = \frac{1}{2} C_1 \left(\frac{V_1}{2}\right)^2$$

$$r = \frac{E_f}{E_0} = \frac{\frac{1}{2} C_1 \left(\frac{V_1}{2}\right)^2}{\frac{1}{2} C_1 V_1^2} = \frac{1}{4}$$

2. [25 points] In the circuit below  $C_1$  represents a touch sensor. The comparator controls the position of the switch as follows: Whenever  $V_o$  reaches the value  $V_{ref}$ , the switch is set to position  $a$ . After  $V_o$  drops to zero, the switch is set to position  $b$ . Touch is detected by measuring the frequency  $f_o$  at which the switch position changes. Derive an analytical expression for  $f_o$ . Assume that the operational amplifier is ideal. Suggestion: sketch  $v_o(t)$  and mark the knowns and unknown in the graph.



$$f_o = \frac{I_1 \cdot I_2}{C \cdot V_{ref} (I_1 + I_2)}$$

The op-amp is in negative feedback.  
 $v_p = v_n = 0$        $v_p = v_n = 0V$

Let's define the current + voltage through  $C_1$  as  $i_c(t)$  +  $v_c(t)$   
 $i = C \frac{dV}{dt} \Rightarrow v_c(t) = \frac{1}{C} \int_0^+ i_c(x) dx + v_c(0)$

Charge Cycle (switch is set to  $b$ )

$$V_{ref} = \frac{1}{C} \int_0^{t_a} i_c(x) dx + v_c(0)$$

$$V_{ref} = \frac{1}{C} I_2 t_a + 0V$$

$$t_a = \frac{C \cdot V_{ref}}{I_2}$$

Discharge Cycle (switch is set to  $a$ )

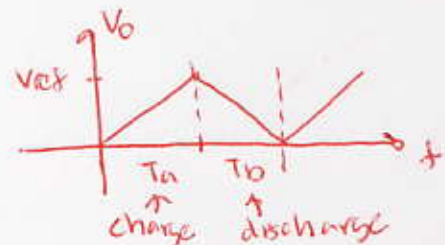
$$0V = \frac{1}{C} \int_{t_a}^{t_a+t_b} i_c(x) dx + v_c(t_a)$$

$$0V = \frac{1}{C} (-I_1) t_b + V_{ref}$$

$$t_b = \frac{C \cdot V_{ref}}{I_1}$$

$$T = t_a + t_b \Rightarrow f = \frac{1}{T} = \frac{1}{t_a + t_b}$$

$$f = \frac{C \cdot V_{ref}}{I_1} + \frac{C \cdot V_{ref}}{I_2} = \frac{I_1 \cdot I_2}{C \cdot V_{ref} (I_1 + I_2)}$$



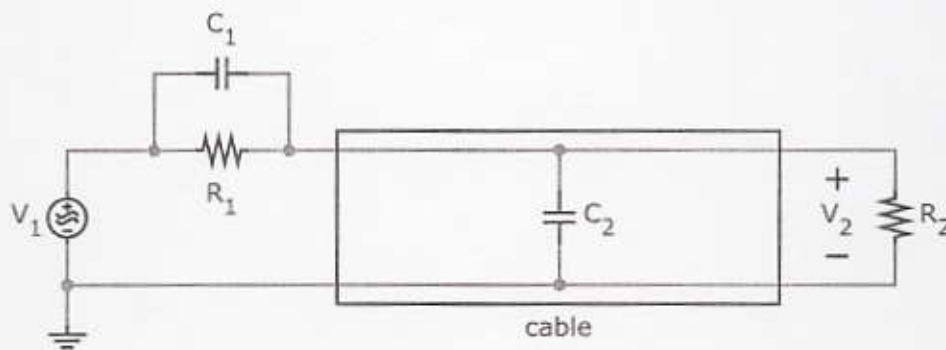
Note:  $C_1$  charges through  $I_2$  + discharges through  $I_1$ .

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3. [25 points] The circuit below shows a simple model of a wired Ethernet connection.  $V_1$  is the signal source and  $R_1$  represents its impedance. The cable is modelled by capacitor  $C_2$  and  $R_2$  represents the receiver's input impedance. The capacitor  $C_1$  has been added to enable higher frequency transmission at low error rates.

Derive an expression for  $C_1$  as a function of  $R_1$ ,  $R_2$ , and  $C_2$  for which  $\frac{V_2(j\omega)}{V_1(j\omega)}$  has a constant value that is independent of frequency.

Note: This technique is used in many transceivers including 100 Mbit Ethernet.



$$C_1 = \frac{C_2 R_2}{R_1}$$

### Short Solution

The impedance at low frequencies should equal the impedance at high frequencies. Since the caps are open at low freqs & shorts at high freqs

$$Z(\omega) = Z(\infty)$$

$$\frac{R_2}{R_1 + R_2} = \frac{\frac{1}{sC_2}}{\frac{1}{sC_1} + \frac{1}{R_2}}$$

$$\frac{R_2}{R_1 + R_2} = \frac{C_1}{C_1 + C_2}$$

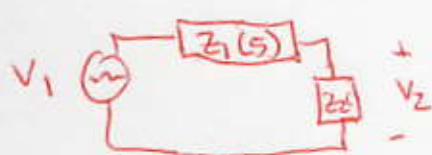
$$R_2 (C_1 + C_2) = C_1 (R_1 + R_2)$$

$$C_1 = \frac{C_2 R_2}{R_1}$$

Prob 5/

### "Long" Solution

- Let's find the transfer function  $V_2(s)/V_1(s)$



$$\frac{V_2(s)}{V_1(s)} = \frac{Z_2(s)}{Z_1(s) + Z_2(s)}$$

Voltage Divider

Where

$$Z_1(s) = \frac{R_1 \cdot \frac{1}{sC_1}}{R_1 + \frac{1}{sC_1}} = \frac{R_1}{1 + sR_1C_1}$$

$$Z_2(s) = \frac{R_2 \cdot \frac{1}{sC_2}}{R_2 + \frac{1}{sC_2}} = \frac{R_2}{1 + sR_2C_2}$$

$$\begin{aligned} \frac{V_2(s)}{V_1(s)} &= \frac{\frac{R_2}{1 + sR_2C_2}}{\frac{R_1}{1 + sR_1C_1} + \frac{R_2}{1 + sR_2C_2}} = \frac{R_2 (1 + sR_1C_1)}{R_1 (1 + sR_2C_2) + R_2 (1 + sR_1C_1)} \\ &= \frac{R_2}{R_1 + R_2} \cdot \frac{(1 + sR_1C_1)}{1 + s \frac{R_1R_2}{R_1 + R_2} (C_1 + C_2)} \end{aligned}$$

In order for the transfer to be independent of frequency, the coefficients of  $s$  must be equal.

$$\therefore R_1 C_1 = \frac{R_1 R_2}{R_1 + R_2} (C_1 + C_2)$$

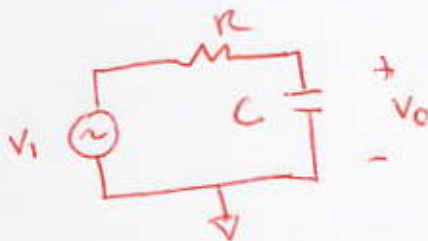
$$R_1 C_1 (R_1 + R_2) = R_1 R_2 (C_1 + C_2)$$

$$C_1 \frac{R_1}{R_1 + R_2} = C_2 \frac{R_2}{R_1 + R_2}$$

$$C_1 = C_2 \frac{R_2}{R_1}$$

4. [25 points] An audio system suffers from high frequency interference. Design a circuit consisting of a resistor  $R$  and capacitor  $C$  that passes low frequency signals ( $\left| \frac{V_o(j\omega)}{V_i(j\omega)} \right|_{\omega=0} = 1$ ) and attenuates high frequency signals ( $\left| \frac{V_o(j\omega)}{V_i(j\omega)} \right|_{\omega>0} < 1$ ).

(a) Draw a diagram of a circuit with these characteristics, consisting of  $R$  and  $C$ . Clearly mark the input and output voltages  $V_i$  and  $V_o$  with plus and minus signs.



$$\frac{V_o}{V_i} = \frac{\frac{1}{sC}}{\frac{1}{sC} + R} = \frac{1}{1 + sRC}$$

(b) Derive a symbolic expression for the value of  $C$  as a function of  $R$  that results in 26 dB attenuation at a given frequency  $f_o$ .  
Hint: draw the Bode plot (piece-wise linear approximation of magnitude response) of the circuit. Mark what is known and unknown in the graph.

$$C = \frac{10}{\pi f_o R} \quad (\text{assume } f_o \text{ is in Hertz}) = \frac{20}{f_o R} \quad (\text{assume } f_o \text{ is in rad/s})$$

Bode Plot for  $H(s) = \frac{1}{1 + sRC} = \frac{1}{1 + s/\omega_p}$  where  $\omega_p = \frac{1}{RC}$



The transfer function of a first-order system is given by  $H(j\omega) = \frac{1}{1 + j\omega RC} = \frac{1}{1 + j\omega/\omega_p}$ . If  $\omega \gg \omega_p$  (large), the imaginary term in the denominator dominates, and we have

$$H(j\omega) \approx \frac{1}{j\omega/\omega_p}$$

$$G_{\text{andB}}(\omega) = 20 \log_{10} |H(j\omega)|$$

Prob 4 cont.

The gain difference at a  $\omega_0$  (frequency) 10 times  $\omega_p$  is

$$\begin{aligned}G_{\text{indB}}(10\omega_p) - G_{\text{indB}}(\omega_p) &= -20 \log_{10}(10\omega_p) + 20 \log_{10}(\omega_p) \\&= -20 \log_{10}(10) - 20 \log_{10}(\omega_p) + 20 \log_{10}(\omega_p) \\&= -20 \log_{10}(10) = \underline{-20 \text{ dB}} \quad (\text{at } 10 \text{ times } \omega_p)\end{aligned}$$

The gain difference at a  $\omega_0$  2 times  $\omega_p$  is

$$\begin{aligned}G_{\text{indB}}(2\omega_p) - G_{\text{indB}}(\omega_p) &= -20 \log_{10}(2\omega_p) + 20 \log_{10}(\omega_p) \\&= -20 \log_{10}(2) - 20 \log_{10}(\omega_p) + 20 \log_{10}(\omega_p) \\&= -20 \log_{10}(2) = -6 \text{ dB} \quad (\text{at } 2 \text{ times } \omega_p)\end{aligned}$$

Now for our problem, we have 26 dB attenuation

$$\begin{aligned}26 \text{ dB} &= \underset{\substack{\uparrow \\ 10x}}{20 \text{ dB}} + \underset{\substack{\uparrow \\ 2x}}{6 \text{ dB}} \\&= G_{\text{indB}}(10x) + G_{\text{indB}}(2x) \\&= G_{\text{indB}}(20 \cdot \omega_p)\end{aligned}$$

$$\omega_0 = 20 \cdot \omega_p = 20 \cdot \frac{1}{RC}$$

$$\Rightarrow C = \frac{20}{R \cdot \omega_0}$$

$$\text{Since } \omega_0 = 2\pi f_0$$

$$C = \frac{20}{2\pi f_0 R} = \boxed{\frac{10}{\pi f_0 R}}$$