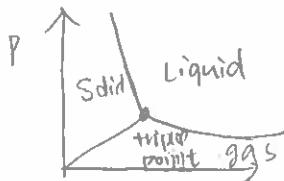


17

1. Short Answer. 3 points each

Note: *questions are underlined - answer all questions.*

- (a) Sketch the P vs. T phase diagram for pure water, identifying solid, liquid, and gas phase regions. Show the two-phase boundaries and triple point.



- (b) Why do we use reference conditions for thermodynamic data like U and H?

1) Energy is relative, not useful to study absolute energy

2) U, H are state variables. Path independent. choose good reference will make calculation easier

- (c) For pure water (equilibrium conditions) at atmospheric pressure and 90°C, can there be any vapor in the system? Why or why not?

Yes. There is vapor liquid equilibrium, So ~~stop~~ some H_2O ~~stop~~ escape liquid phase and stay as vapor (vapor pressure of H_2O)

- (d) For ideal gases, liquids and solids, how does internal energy depend on pressure?

gas: ΔU not a function of P , no effect.

liquid/solid: ΔU not a function of P , no effect.

- (e) Write the Gibbs phase rule, identifying the terms and give one example for a pure component (e.g. water).

$$\Delta F = 2 + C - \pi$$

C : # of components

π : # of phases

pure water, lig + vap phase

$$\Delta F = 2 + 1 - 2 = \frac{1}{2} \rightarrow \text{need specifying temperature}$$

- (f) At the liquid water - water vapor boundary in the presence of air (temperature T, pressure P), what is the mole fraction of air at the interface in terms of the water vapor pressure $P^*(T)$? What 'laws' are used for this analysis?

$$P_{\text{H}_2\text{O}} = P^*_{\text{H}_2\text{O}}(T) = y_{\text{H}_2\text{O}} \cdot P \quad P = x_{\text{H}_2\text{O}} \cdot P^*_{\text{H}_2\text{O}}(T)$$

$$y_{\text{H}_2\text{O}} = \frac{x_{\text{H}_2\text{O}} \cdot P^*_{\text{H}_2\text{O}}(T)}{P} = \frac{1 \cdot P^*(T)}{P}$$

$$y_{\text{air}} = 1 - y_{\text{H}_2\text{O}} = 1 - \frac{P^*(T)}{P}$$

→ Raoult's law

- (g) For a gas with 2 mole percent of some vapor component in contact with liquid water at 20°C and 3 atm, estimate the mole fraction of this component in water if the Henry's law coefficient is 6×10^4 atm/mole fraction.

Henry's:

$$P_A = y_A \cdot P_{\text{tot}} = x_A \cdot H_A(T)$$

$$x_A = \frac{y_A \cdot P_{\text{tot}}}{H_A(T)} = \frac{0.02 \times 3 \text{ atm}}{6 \times 10^4 \text{ atm/mole fraction}} = 1 \times 10^{-5} \text{ mole fraction}$$

$$y_A = 0.02$$

$$T = 20^\circ\text{C} \quad P = 3 \text{ atm}$$

$$= 1 \times 10^{-5} \text{ mole fraction}$$

- (h) Write the energy balance equations (assuming steady state) for a closed system and an open system, defining all terms. Include your assumptions regarding the sign conventions for heat and work.

closed: $\Delta U + \Delta E_k + \Delta E_p = Q - W \rightarrow \text{CSNdt}$

heat: into sys "+"
out sys. "-"

open $\dot{\Delta H} + \dot{\Delta E_k} + \dot{\Delta E_p} = \dot{Q} - \dot{W}_{\text{shaft}}$

work done by system "+"
done on sys "-"

- (i) What are the defining equations for heat capacity at constant volume and heat capacity at constant pressure?

$$C_V = \left(\frac{dU}{dT} \right)_V$$

$$C_P = \left(\frac{dH}{dT} \right)_P$$

- (j) What does it mean to say the internal energy is a 'state variable'?

it's path-independent. Only difference counts, doesn't

matter where it starts..

X5

2. (30 Points)

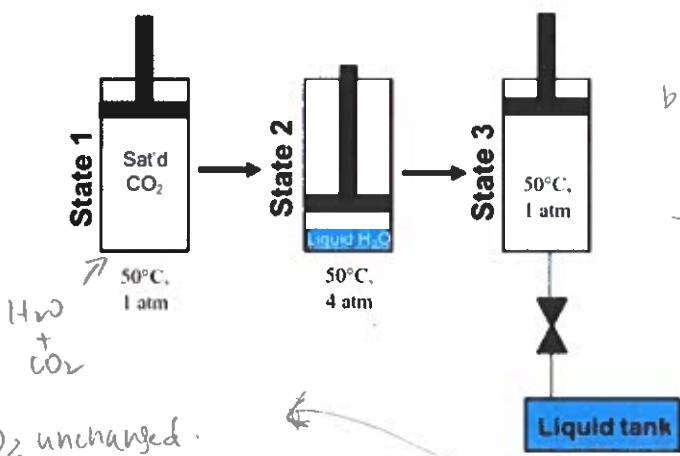
Useful information:

Antoine's Equation Parameters for water (P in mmHg, T in °C): A: 8.07131, B: 1730.63, C: 233.426

Antoine's Equation: $\log(P^*) = A - B/(T+C)$

1 atm = 760 mmHg = 1.01325 bar

(a) [15 points] A cylinder is charged with water-saturated CO₂ at 50°C and 1 atm. The partial pressures are: p_{CO₂}=723.2 mmHg, p_{H₂O}=36.8 mmHg. The cylinder is compressed isothermally to 4 atm. A liquid take-out valve is opened and the liquid water is drained out. The cylinder is then returned to 50°C and 1 atm. What percentage of water vapor condenses in State 2?



State 1:

$P_{CO_2} = y_{CO_2} \cdot P_{tot} \Rightarrow y_{CO_2} = 0.952$

$y_{H_2O} = 0.048$

basis: 952 mol CO₂
→ 48 mol H₂O

State 2:

$P_{H_2O}^*(50^\circ\text{C}) = 10$
 $= 92.3 \text{ mmHg}$

Isothermally → Equilibrium
Raoult's law

$P_{H_2O} = y_{H_2O} \cdot P_{tot} = x_{H_2O} \cdot P_{H_2O}^*$

$y_{H_2O} = \frac{x_{H_2O} \cdot P_{H_2O}^*}{P_{tot}} = \frac{1 \cdot 92.3 \text{ mmHg}}{760 \text{ mmHg} \times 4}$
 $= 0.0303$

CO₂ unchanged.(CO₂ = constant)

$n_{tot} (1 - 0.0303) = 952 \text{ mol}$

$n_{CO_2} = 921.8 \text{ mol}$

$n_{H_2O, \text{vapor}} = 29.8 \text{ mol}$

% condense: $\frac{48 - 29.8}{48} \times 100\% = 37.9\%$

(b) [5 points] What is the dew point temperature in State 3?

State 3: $y_{CO_2} = 0.9697$

$y_{H_2O} = 0.0303$

$P_{H_2O} = 0.0303 \cdot 1 \text{ atm} = 0.0303 \text{ atm} = 23.028 \text{ mmHg} = P_{H_2O}^* (\text{dew point})$

$\log_{10}(23.028) = 8.07131 - \frac{1730.63}{233.426 + T_{dp}}$

Solve for T_{dp} to get the solution

T_{dp}

X4

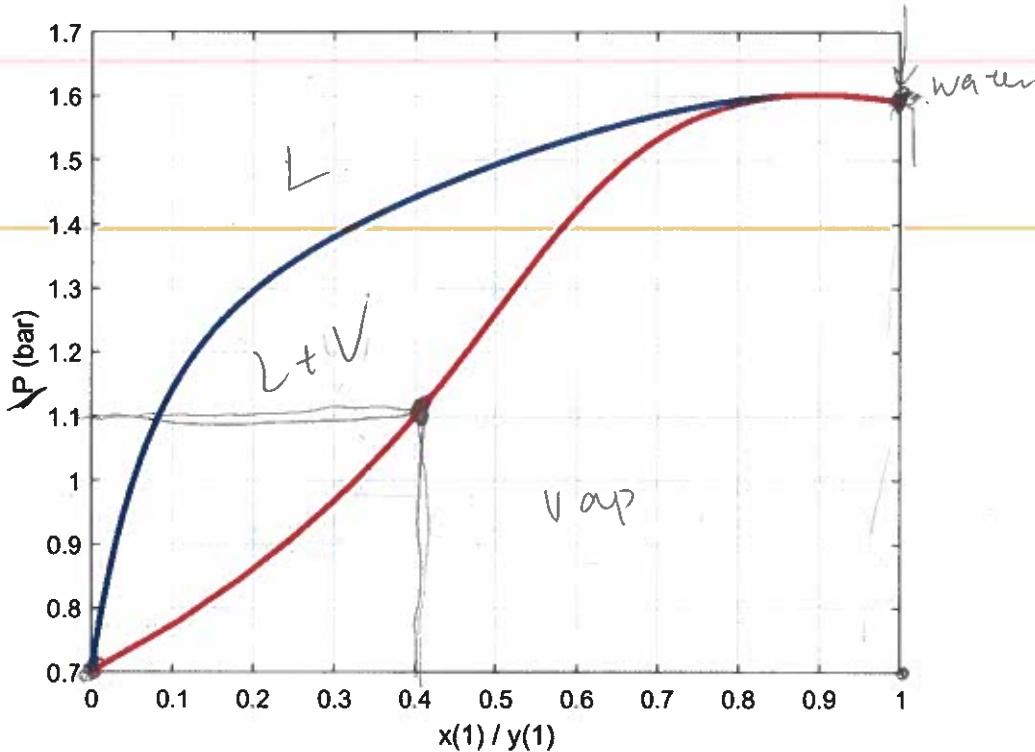
Useful information:

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B: 1730.63, C: 233.426

Antoine's Equation: $\log(P^*) = A - B/(T+C)$

1 atm = 760 mmHg = 1.01325 bar



- (c) [5 points] The diagram above describes the pressure versus composition of an ethanol/water mixture at 90°C . It is unknown which component is which (whether component 1 is ethanol or water). Find out what component 1 is and show the calculations you used to decide this. (No credit will be given for guesses without any work).

100% x_1 $90^\circ\text{C} \quad P_{\text{litro}}^*(90^\circ\text{C}) = 10$ Antoine eq
compare result with diag

- (d) [5 points] You have an ethanol/water mixture at a pressure of 1.1 bar and a composition of 0.4 (for component 1). How many degrees of freedom are there with this system?

$$\begin{aligned} \text{dof} &= 2 + C - \pi \\ &= 2 + 2 - 2 \end{aligned}$$

$$= 2$$

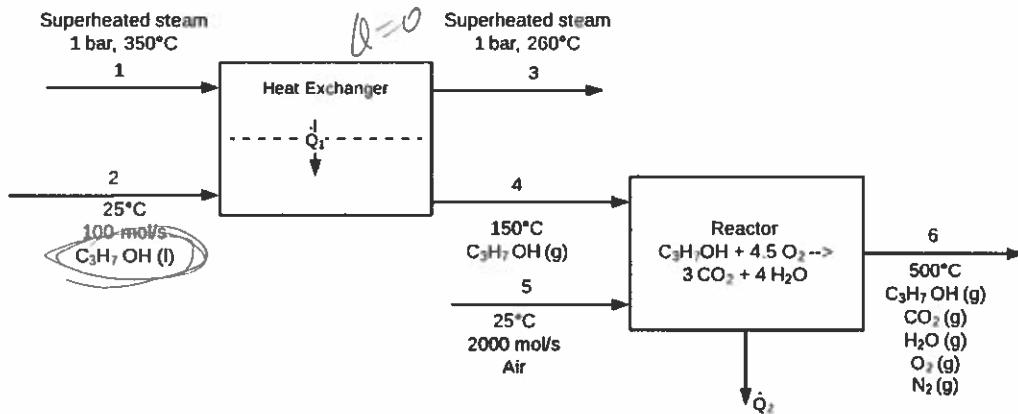
x_1
 y_1

5 \Rightarrow 0 dof overall

X7

3. (40 Points)

Consider the flow diagram below:



(a) [15 points] Solve for the heat transferred to stream 4 (\dot{Q}_1) and the flowrate of steam in stream 1. The heat exchanger is adiabatic. Liquid n-propyl alcohol (C_3H_7OH) has a heat capacity of $150 \text{ J/mol } ^\circ\text{C}$, and gaseous C_3H_7OH has a heat capacity of $80 \text{ J/mol } ^\circ\text{C}$. C_3H_7OH boils at 97°C . The heat of vaporization C_3H_7OH is 50 kJ/mol . Steam tables are included below.

Table B.7 Properties of Superheated Steam^a

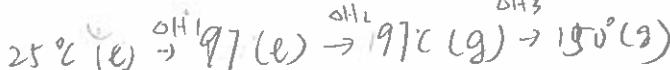
$P(\text{bar})$ ($T_{\text{sat.}} (\text{°C})$)	Sat'd Water		Temperature ($^\circ\text{C}$) →								
	\dot{H}	\dot{U}	50	75	100	150	200	250	300	350	
0.0	\dot{H}	—	—	2595	2642	2689	2784	2880	2978	3077	3177
(-)	\dot{U}	—	—	2446	2481	2517	2589	2662	2736	2812	2890
0.1	\dot{H}	191.8	2584.8	2593	2640	2688	2783	2880	2977	3077	3177
(45.8)	\dot{U}	191.8	2438.0	2444	2480	2516	2588	2661	2736	2812	2890
	\dot{V}	0.00101	14.7	14.8	16.0	17.2	19.5	21.8	24.2	26.5	28.7
0.5	\dot{H}	340.6	2646.0	209.3	313.9	2683	2780	2878	2979	3076	3177
(81.3)	\dot{U}	340.6	2484.0	209.2	313.9	2512	2586	2660	2735	2811	2889
	\dot{V}	0.00103	3.24	0.00101	0.00103	3.41	3.89	4.35	4.83	5.29	5.75
1.0	\dot{H}	417.5	2675.4	209.3	314.0	2676	2776	2875	2975	3074	3176
(99.6)	\dot{U}	417.5	2506.1	209.2	313.9	2507	2583	2658	2734	2811	2889
	\dot{V}	0.00104	1.69	0.00101	0.00103	1.69	1.94	2.17	2.40	2.64	2.87
5.0	\dot{H}	640.1	2747.5	209.7	314.3	419.4	632.2	2855	2961	3065	3168
(151.8)	\dot{U}	639.6	2560.2	209.2	313.8	418.8	631.6	2643	2724	2803	2883
	\dot{V}	0.00109	0.375	0.00101	0.00103	0.00104	0.00109	0.425	0.474	0.522	0.571

^a Adapted from R. W. Haywood, *Thermodynamic Tables in SI (Metric) Units*, Cambridge University Press, London, 1968. Water is a liquid in the enclosed region between 50°C and 350°C . \dot{H} = specific enthalpy (kJ/kg), \dot{U} = specific internal energy (kJ/kg), \dot{V} = specific volume (m³/kg). Note: $\text{kJ/kg} \times 0.4303 = \text{Btu/lb}_{\text{m}}$.

D) ~~Balance $\Delta H + Q_{\text{ext}} + \dot{H}_{\text{ext}} = 0$~~ ^{ad iation}

$$\Rightarrow \Delta H_{\text{tot}} = 0$$

\rightarrow II Energy needed



$\Delta H = Q$ (within react.)

$$\Delta H_1 = 100 \frac{\text{mol}}{\text{s}} \cdot \frac{150 \text{ J}}{\text{mol} \cdot \text{K}} \cdot (97 - 25)^\circ\text{C} =$$

$$\Delta H_2 = 100 \frac{\text{mol}}{\text{s}} \times 50 \frac{\text{J}}{\text{mol}} =$$

$$\Delta H_3 = 100 \frac{\text{mol}}{\text{s}} \times 80 \frac{\text{J}}{\text{mol}} \times (150 - 97)^\circ\text{C} =$$

$$\Delta H_{C_3H_7OH} + \Delta H_{\text{gas}} = 0$$

$$\Delta H_{C_3H_7OH} = 6504 \frac{\text{kJ}}{\text{s}}$$

$$\Delta H_{\text{gas}} = 0$$

$$\Delta H_{C_3H_7OH} + \Delta H_{\text{gas}} = 0$$

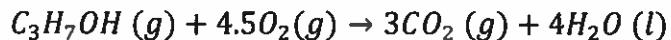
$$\Delta H_{\text{gas}} = -6504 \frac{\text{kJ}}{\text{s}}$$

$$\Delta H = m(\hat{H}_{\text{out}} - \hat{H}_{\text{in}}) = -6504 \frac{\text{kJ}}{\text{s}} \quad \hat{H}_{260} = 2975 + 0.2(3074 - 25)$$

$$6 \quad \dot{m} = -\frac{6504 \text{ kJ/s}}{(2994.8 - 3176) \text{ kJ/s}} = 2994.8$$

$$\dot{m}_{\text{gas}} = \frac{35894.1 \text{ kg/s}}{3}$$

(b) [20 points] If conversion is 80% what is composition and molar flowrate of stream 6? How much heat must be removed from the reactor (\dot{Q}_2)? The specific standard heat of reaction ($\Delta\bar{H}_r^\circ$) is -1000 kJ/mol. The heat of vaporization of water is 60 kJ/mol. Heat capacities are included below.



	$C_3H_7OH(l)$	$C_3H_7OH(g)$	$O_2(g)$	$N_2(g)$	$H_2O(l)$	$H_2O(g)$	$CO_2(g)$
$C_p(J/mol \cdot ^\circ C)$	150	80	30	25	100	36	50



1) cool rxn to $25^\circ C$.

$$\Delta H_2 = 6504 \frac{KJ}{S}$$

2) heat from reaction.

$$\Delta H = 100 \frac{mol}{S} \cdot -\frac{1000 \text{ kJ}}{mol}$$

$$\Delta H_2 = -10^5 \frac{KJ}{mol}$$

3) heat products to $500^\circ C$

80% conversion; product stream:

$$n_{C_3H_7OH} = 20 \text{ mol/s}$$

$$n_{CO_2} = 80 \cdot 3 = 240 \text{ mol/s}$$

$$n_{H_2O} = 4 \cdot 80 = 320 \text{ mol/s}$$

$$n_{O_2} = 2000 \cdot 0.81 \cdot (24.5)(0.2) = 378 \cdot \text{mol/s}$$

$$n_{N_2} = 1580 \text{ mol/s}$$

Cpi in table.
ni calculated

$$\dot{H}_3 = \sum n_i \cdot \int_{25^\circ C}^{500^\circ C} C_{pi} dT$$

=) next calculate

(c) **EXTRA CREDIT:** (5 points) The vapor leaving the reactor is fed to a turbine and leaves the turbine with an outlet temperature of $110^\circ C$. How much work you can produce?

