

## 5.104

Oxygen at 300 kPa, 100°C is in a piston/cylinder arrangement with a volume of 0.1 m<sup>3</sup>. It is now compressed in a polytropic process with exponent,  $n = 1.2$ , to a final temperature of 200°C. Calculate the heat transfer for the process.

Solution:

Continuity:  $m_2 = m_1$

Energy Eq.5.11:  $m(u_2 - u_1) = {}_1Q_2 - {}_1W_2$

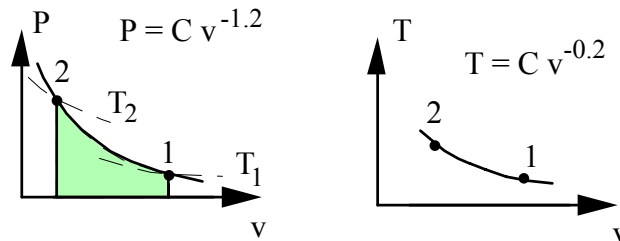
State 1:  $T_1$ ,  $P_1$  & ideal gas, small change in  $T$ , so use Table A.5

$$\Rightarrow m = \frac{P_1 V_1}{RT_1} = \frac{300 \times 0.1 \text{ m}^3}{0.25983 \times 373.15} = 0.309 \text{ kg}$$

Process:  $PV^n = \text{constant}$

$$\begin{aligned} {}_1W_2 &= \frac{1}{1-n} (P_2 V_2 - P_1 V_1) = \frac{mR}{1-n} (T_2 - T_1) = \frac{0.309 \times 0.25983}{1 - 1.2} (200 - 100) \\ &= -40.2 \text{ kJ} \end{aligned}$$

$$\begin{aligned} {}_1Q_2 &= m(u_2 - u_1) + {}_1W_2 \cong mC_v(T_2 - T_1) + {}_1W_2 \\ &= 0.3094 \times 0.662 (200 - 100) - 40.2 = \mathbf{-19.7 \text{ kJ}} \end{aligned}$$



**10-85** A combined gas-steam power cycle uses a simple gas turbine for the topping cycle and simple Rankine cycle for the bottoming cycle. The mass flow rate of air for a specified power output is to be determined.

**Assumptions 1** Steady operating conditions exist. **2** The air-standard assumptions are applicable for Brayton cycle. **3** Kinetic and potential energy changes are negligible. **4** Air is an ideal gas with constant specific heats.

**Properties** The properties of air at room temperature are  $c_p = 1.005 \text{ kJ/kg}\cdot\text{K}$  and  $k = 1.4$  (Table A-2a).

**Analysis** Working around the topping cycle gives the following results:

$$T_{6s} = T_5 \left( \frac{P_6}{P_5} \right)^{(k-1)/k} = (293 \text{ K})(8)^{0.4/1.4} = 530.8 \text{ K}$$

$$\eta_C = \frac{h_{6s} - h_5}{h_6 - h_5} = \frac{c_p(T_{6s} - T_5)}{c_p(T_6 - T_5)}$$

$$\begin{aligned} \longrightarrow T_6 &= T_5 + \frac{T_{6s} - T_5}{\eta_C} \\ &= 293 + \frac{530.8 - 293}{0.85} = 572.8 \text{ K} \end{aligned}$$

$$T_{8s} = T_7 \left( \frac{P_8}{P_7} \right)^{(k-1)/k} = (1373 \text{ K}) \left( \frac{1}{8} \right)^{0.4/1.4} = 758.0 \text{ K}$$

$$\begin{aligned} \eta_T &= \frac{h_7 - h_8}{h_7 - h_{8s}} = \frac{c_p(T_7 - T_8)}{c_p(T_7 - T_{8s})} \longrightarrow T_8 = T_7 - \eta_T(T_7 - T_{8s}) \\ &= 1373 - (0.90)(1373 - 758.0) \\ &= 819.5 \text{ K} \end{aligned}$$

$$T_9 = T_{\text{sat}@6000 \text{ kPa}} = 275.6^\circ\text{C} = 548.6 \text{ K}$$

Fixing the states around the bottom steam cycle yields (Tables A-4, A-5, A-6):

$$h_1 = h_{f@20 \text{ kPa}} = 251.42 \text{ kJ/kg}$$

$$v_1 = v_{f@20 \text{ kPa}} = 0.001017 \text{ m}^3/\text{kg}$$

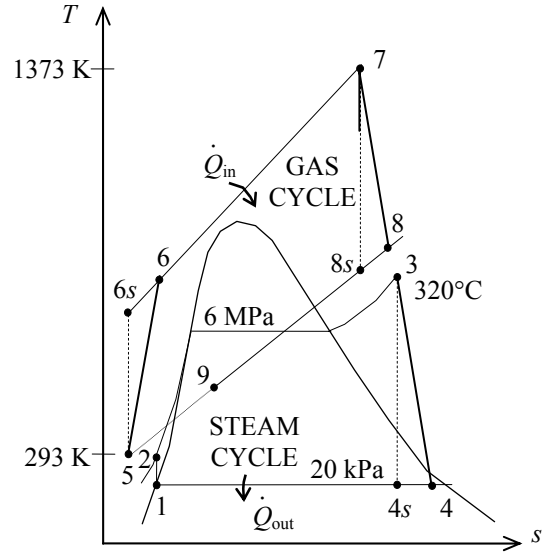
$$\begin{aligned} w_{p,\text{in}} &= v_1(P_2 - P_1) \\ &= (0.001017 \text{ m}^3/\text{kg})(6000 - 20) \text{ kPa} \left( \frac{1 \text{ kJ}}{1 \text{ kPa}\cdot\text{m}^3} \right) \\ &= 6.08 \text{ kJ/kg} \end{aligned}$$

$$h_2 = h_1 + w_{p,\text{in}} = 251.42 + 6.08 = 257.5 \text{ kJ/kg}$$

$$\left. \begin{array}{l} P_3 = 6000 \text{ kPa} \\ T_3 = 320^\circ\text{C} \end{array} \right\} \begin{array}{l} h_3 = 2953.6 \text{ kJ/kg} \\ s_3 = 6.1871 \text{ kJ/kg}\cdot\text{K} \end{array}$$

$$\left. \begin{array}{l} P_4 = 20 \text{ kPa} \\ s_4 = s_3 \end{array} \right\} h_{4s} = 2035.8 \text{ kJ/kg}$$

$$\begin{aligned} \eta_T &= \frac{h_3 - h_4}{h_3 - h_{4s}} \longrightarrow h_4 = h_3 - \eta_T(h_3 - h_{4s}) \\ &= 2953.6 - (0.90)(2953.6 - 2035.8) \\ &= 2127.6 \text{ kJ/kg} \end{aligned}$$



The net work outputs from each cycle are

$$\begin{aligned}
 w_{\text{net, gas cycle}} &= w_{T,\text{out}} - w_{C,\text{in}} \\
 &= c_p (T_7 - T_8) - c_p (T_6 - T_5) \\
 &= (1.005 \text{ kJ/kg} \cdot \text{K})(1373 - 819.5 - 572.7 + 293)\text{K} \\
 &= 275.2 \text{ kJ/kg}
 \end{aligned}$$

$$\begin{aligned}
 w_{\text{net, steam cycle}} &= w_{T,\text{out}} - w_{P,\text{in}} \\
 &= (h_3 - h_4) - w_{P,\text{in}} \\
 &= (2953.6 - 2127.6) - 6.08 \\
 &= 819.9 \text{ kJ/kg}
 \end{aligned}$$

An energy balance on the heat exchanger gives

$$\dot{m}_a c_p (T_8 - T_9) = \dot{m}_w (h_3 - h_2) \longrightarrow \dot{m}_w = \frac{c_p (T_8 - T_9)}{h_3 - h_2} \dot{m}_a = \frac{(1.005)(819.5 - 548.6)}{2953.6 - 257.5} = 0.1010 \dot{m}_a$$

That is, 1 kg of exhaust gases can heat only 0.1010 kg of water. Then, the mass flow rate of air is

$$\dot{m}_a = \frac{\dot{W}_{\text{net}}}{w_{\text{net}}} = \frac{100,000 \text{ kJ/s}}{(1 \times 275.2 + 0.1010 \times 819.9) \text{ kJ/kg air}} = \mathbf{279.3 \text{ kg/s}}$$