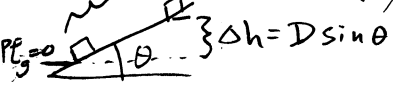


Mike Dewese MT2

4. a.) $PE_{sp} = \frac{1}{2} k \Delta X^2 = \boxed{\frac{1}{2} k (L-l)^2}$

b.) c.o.E.: $(KE_f + PE_{sp,f} + PE_{g,f})_f - (KE_i + PE_{sp,i} + PE_{g,i})_i = W_{ext}$
 (no friction)
 $mgD \sin \theta - \frac{1}{2} k (L-l)^2 = 0$



$$D = \frac{k(L-l)^2}{2mg \sin \theta}$$

c.) $W_g = \vec{F}_g \cdot \Delta \vec{r}_{block} = \boxed{-mg \sin \theta (L-l)}$



d.) $\vec{J} = \Delta \vec{P} = \vec{P}_f - \vec{P}_i$ — (1)



c.o.E. $(\frac{1}{2} m v_f^2 + mg(L-l) \sin \theta)_f - (\frac{1}{2} k (L-l)^2)_i = W_{ext}$

$$v_f = \sqrt{-2g(L-l) \sin \theta + \frac{k}{m} (L-l)^2} \quad \text{--- (2)}$$

(2) in (1) $\Rightarrow \boxed{\vec{J} = m \sqrt{-2g(L-l) \sin \theta + \frac{k}{m} (L-l)^2} \hat{i}}$

e.) c.o.E. $(KE_f + PE_{sp} + mgD' \sin \theta)_f - (KE_i + \frac{1}{2} k (L-l)^2 + PE_{g,i})_i = -D' \mu_k F_N$
 \vec{J} points up the slope

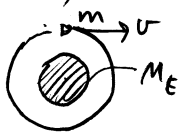
N2L y: $F_N - mg \cos \theta = m a_y \Rightarrow F_N = mg \cos \theta$ — (4)

(4) in (3) $\Rightarrow mgD' \sin \theta - \frac{1}{2} k (L-l)^2 = -D' \mu_k mg \cos \theta$

$$D' mg (\sin \theta + \mu_k \cos \theta) = \frac{1}{2} k (L-l)^2$$

$$\boxed{D' = \frac{k(L-l)^2}{2mg(\sin \theta + \mu_k \cos \theta)}}$$

2. a.) uniform circular motion; $a_y = -\frac{v^2}{r} = -\frac{v^2}{2R}$



↑ NZL projectile y: $F_{net,y} = ma_y$

$$-\frac{GM_E m}{(2R)^2} = m\left(-\frac{v^2}{2R}\right)$$

$$v = \sqrt{\frac{GM_E}{2R}}$$

b.) $T = \frac{2\pi(2R)}{v} = 4\pi R \sqrt{\frac{2R}{GM_E}}$

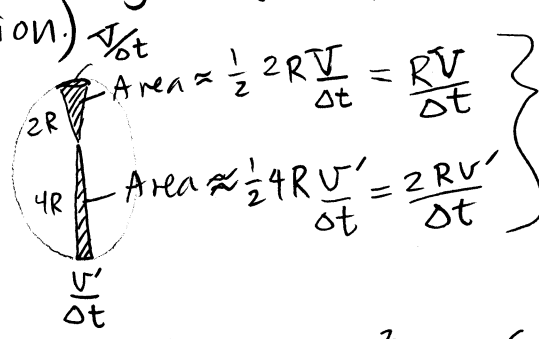
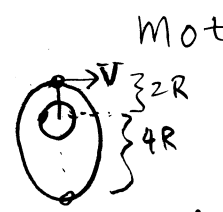
c.) C.O.E.: $\left(-G \frac{M_E m}{r_{max}} + k \cancel{E}_f\right)_f - \left(-\frac{GM_E m}{2R} + \frac{1}{2} m \frac{GM_E}{2R}\right)_i = 0$

$$\frac{1}{r_{max}} = \frac{1}{4R}$$

$$r_{max} = 4R$$

d.) K2L: equal area is swept out by a line connecting the sun (or Earth in this case) and a given planet (or projectile) at any point in its orbit.

(OR: Conservation of angular momentum: Central forces such as gravity can't exert a torque on the orbiting object, so $\vec{L} = \text{const.}$ Throughout the motion.)



$$\left. \begin{aligned} \text{Area} &\approx \frac{1}{2} 2R \frac{v}{dt} = \frac{Rv}{dt} \\ \text{Area} &\approx \frac{1}{2} 4R \frac{v'}{dt} = \frac{2Rv'}{dt} \end{aligned} \right\} v' = \frac{v}{2} \quad \text{OR: C.O.L.} \\ v 2R = v' 4R \Rightarrow v' = \frac{v}{2}$$

C.O.E. $-\frac{GM_E m}{2R} + \frac{1}{2} m v^2 = -\frac{GM_E m}{4R} + \frac{1}{2} m \frac{v^2}{4}$

$$\frac{13}{24} v^2 = \frac{GM_E}{4R}$$

$$v = \sqrt{\frac{2}{3} \frac{GM_E}{R}}$$

e.) K3L: $\frac{a_1^3}{T_1^2} = \frac{a_2^3}{T_2^2}$ } $\frac{(3R)^3}{T^2} = \frac{(6R)^3}{(1 \text{ day})^2}$ } $T = \left(\frac{1}{2}\right)^{3/2} \text{ days} = \frac{1}{2\sqrt{2}} \text{ days}$

3. a.) c.o.P.

$$M(v_{s,x} - v) + 2Mv_{s,x} = 0$$

$$3v_{s,x} = v$$

$$v_{s,x} = \boxed{\frac{1}{3}v}$$

b.) $M(v'_{s,x} - v) + Mv'_{s,x} = 2M \frac{1}{3}v$

$$2v'_{s,x} = \left(\frac{2}{3} + 1\right)v$$

$$v'_{s,x} = \boxed{\frac{5}{6}v}$$

c.) $M(v''_{s,x} + v) + Mv''_{s,x} = 2M \frac{1}{3}v$

↑
boy jumps
rightward

$$2v''_{s,x} = \left(\frac{2}{3} - 1\right)v$$

$$v''_{s,x} = \boxed{-\frac{1}{6}v} < 0 \Rightarrow \text{sled moves to left in diagram}$$

d.) c.o.P. $2Mv_{s,xf} = Mv + M \vec{0}$

$$v_{s,xf} = \boxed{\frac{1}{2}v}$$

↑
snow is initially at rest

e.) variable mass problem: $(dm) + (M) \vec{v} \rightarrow (M+dm) \vec{v} + d\vec{v}$

$$d\vec{p} = (M+dm)(\vec{v} + d\vec{v}) - dm\vec{u} - M\vec{v}$$

$$= \cancel{M\vec{v}} + dm\vec{v} + M d\vec{v} + \cancel{dm d\vec{v}} - dm\vec{u} - \cancel{M\vec{v}}$$

$$= M d\vec{v} - (\vec{u} - \vec{v}) dm$$

$$\vec{F}_{ext} = \frac{d\vec{p}}{dt} = M \frac{d\vec{v}}{dt} - (\vec{u} - \vec{v}) \frac{dM}{dt}$$

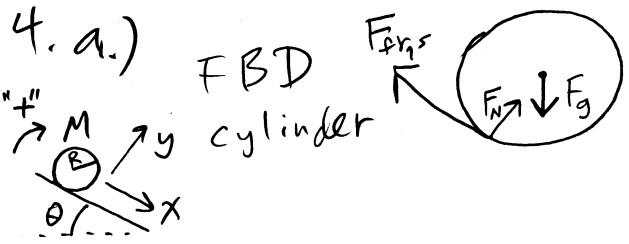
$$F_{ext,x} = 0 \Rightarrow 0 = M \frac{dv_x}{dt} - (u_x - v_x) \frac{dM}{dt}$$

$$\int_{v_{0,x}}^{v_{f,x}} dv = \int_{M_0}^{M_f} \frac{dM}{M} v_{sb}$$

relative
velocity of snowballs w/r sled = const
= v_{sb}

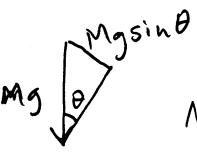
$$v_f - 0 = v_{sb} \ln\left(\frac{M_f}{M_0}\right) = -v_{sb} \ln\left(\frac{2M}{3M}\right) = \boxed{v_{sb} \ln\left(\frac{3}{2}\right)}$$

snowballs thrown leftward



b.) N2L x: $F_{net,x} = M a_{cm,x}$

$$F_{N,x} + Mg \sin \theta - F_{fr,s} = M a_{cm,x} \quad (1)$$



N2L alpha: $\tau_{net,cm} = I_{cm} \alpha$

$$\tau_{N,cm} + \tau_{g,cm} + F_{fr,s} R = \frac{1}{2} M R^2 \alpha \quad (2)$$

rolling without slipping: $a_{cm,x} = + R \alpha \quad (3)$

(1) & (3) = $Mg \sin \theta - F_{fr,s} = M R \alpha \quad (4)$

(2) & (4) => $(Mg \sin \theta - M R \alpha) R = \frac{1}{2} M R^2 \alpha$

$$\alpha \frac{3}{2} R = g \sin \theta$$

$$\alpha = \frac{2}{3} \frac{g \sin \theta}{R} > 0 \Rightarrow \alpha \text{ is clockwise} \quad (5)$$

c.) static friction: $F_{fr,s} \leq \mu_s F_N \quad (6)$

N2L y: $F_N - Mg \cos \theta = M a_{y,cm} \Rightarrow F_N = Mg \cos \theta \quad (7)$

(2) & (5) => $F_{fr,s} = \frac{1}{2} M R \frac{2}{3} \frac{g \sin \theta}{R} = \frac{1}{3} M g \sin \theta \quad (8)$

(6) & (7) & (8) => $\frac{1}{3} M g \sin \theta \leq \mu_s M g \cos \theta$

$$\mu_s \geq \frac{1}{3} \frac{\sin \theta}{\cos \theta} = \frac{1}{3} \tan \theta$$

d.) C.O.E.: $(KE_{tot,f} + Mgh_f) - (KE_{tot,i} + Mgh_i) = \text{ext}$

$F_{fr,s}$ does no work since point of contact is not moving

$$\frac{1}{2} M v_{cm,f}^2 + \frac{1}{2} I_{cm} \omega_f^2 - M g D \sin \theta = 0 \quad (9)$$

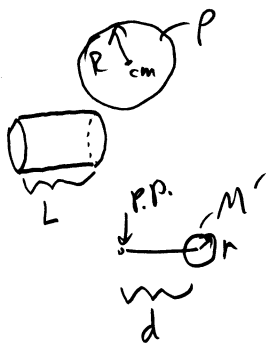
rolling without slipping => $v_{cm,f} = R \omega_f \quad (10)$

(9) & (10) => $\frac{1}{2} M v_{cm,f}^2 + \frac{1}{2} \frac{1}{2} M R^2 \frac{v_{cm,f}^2}{R^2} = M g D \sin \theta$

$$\frac{3}{4} v_{cm,f}^2 = g D \sin \theta \Rightarrow v_{cm,f} = \sqrt{\frac{4}{3} g D \sin \theta}$$



4. e.) I_{cm} of solid cylinder w/ uniform density ρ , radius R



$$I_{cm \text{ solid cylinder}} = \frac{1}{2} M R^2 = \frac{1}{2} (\rho \pi R^2 L) R^2 = \frac{1}{2} \pi \rho L R^4$$

parallel axis theorem

$$I_{pp \text{ solid cylinder}} \stackrel{\Downarrow}{=} I_{cm} + M' d^2 = \frac{1}{2} (\rho \pi r^2 L) r^2 + (\rho \pi r^2 L) d^2 = \rho \pi r^2 L \left(\frac{r^2}{2} + d^2 \right)$$

so for cylinder with 2 holes drilled out:



$$I_{cm} = I_{cm \text{ solid cylinder}} - 2 I_{pp \text{ small solid cylinder}}$$

$$= \frac{1}{2} \pi \rho L R^4 - 2 \rho \pi r^2 L \left(\frac{r^2}{2} + d^2 \right)$$

$$= \boxed{\rho L \pi \left(\frac{R^4}{2} - r^4 - 2 r^2 d^2 \right)}$$