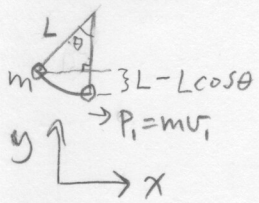


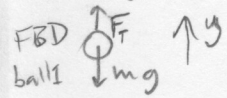
1. a.) cons. of E: $\frac{1}{2} m v_i^2 = mg\Delta h = mg(L - L\cos\theta)$

$$1 - \cos\theta = \frac{v_i^2}{2gL}$$



$$\theta = \cos^{-1}\left(1 - \frac{P_i^2}{2gLm^2}\right)$$

b.) NZL_y: $F_T - mg = ma_y = m\left(\frac{v_i^2}{L}\right) = \frac{P_i^2}{mL}$



$$F_T = mg + \frac{P_i^2}{mL}$$

c.) $\theta \ll 1$: harmonic oscillator: $\omega = \sqrt{g/L}$ $f = \frac{\omega}{2\pi} = \frac{1}{2\pi}\sqrt{g/L}$

time to swing down = $\frac{T}{4} = \frac{1}{4f} = \frac{\pi}{2}\sqrt{L/g}$

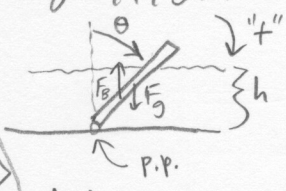
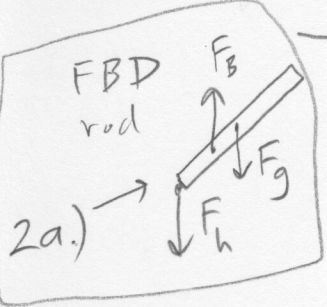
d.) elastic collision: cons. of KE & cons. of $P_x \Rightarrow v_{5f} = v_{1i} = \frac{P_1}{m}$ (F_T acts vertically, so $F_T \cdot v = 0$ no power from tension)
 in fact, since we are told that only the fifth ball is moving after the collision, cons. of momentum is enough to get $v_{5f} = v_{1i}$, since mass of each ball is the same

e.) partially inelastic collision:

cons. of P_x : $m v_{1i} = m v_{4f} + m v_{5f} \Rightarrow v_{5f} = v_{1i} - v_{4f} = \frac{3}{4} v_{1i} = \frac{3}{4} \frac{P_1}{m}$

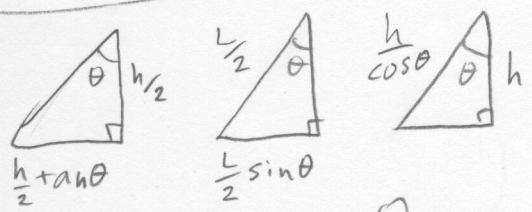
2 b.) static equilibrium while vertical:

for $\theta > 0$:



NZL_x: $\sum \tau = I_{end} \alpha \rightarrow 0$ static
 hinge = P.P.
 $-\frac{h}{2} \tan(\theta) F_B + \frac{L}{2} \sin(\theta) \rho_R L A g = 0$

(1) $\Rightarrow \frac{h}{2} \tan(\theta) \frac{hA}{\cos\theta} \rho_w = \frac{L}{2} \sin(\theta) \rho_R L A g$
 $\cos^2 \theta = \frac{h^2}{L^2} \frac{\rho_w}{\rho_R}$ (3)



$F_B = \frac{hA}{\cos\theta} g \rho_w$ (1)

vertical $\Rightarrow \theta = 0 \Rightarrow \frac{h^2}{L^2} \frac{\rho_w}{\rho_R} = 1$

so $\rho_{R,max} = \frac{h^2}{L^2} \rho_w$ (2)

check balance of forces is satisfied:

NZL_y: $F_B - F_g - F_h = m a_y \rightarrow 0$ static
 $\theta = 0$
 static eq: $F_{h,y} \leq 0$
 so: $F_B \geq F_g$

$\frac{hA}{\cos\theta} \rho_w \geq L A g \rho_R$
 $\rho_R \leq \frac{h}{L} \rho_w$, which is always satisfied if (2) is true. ✓

c.) (3): $\theta = \cos^{-1}\left(\frac{h}{L} \sqrt{\frac{\rho_w}{\rho_R}}\right)$

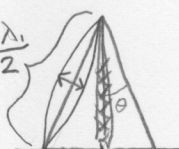
d.) NZL_y: $-F_h + F_B - F_g = m a_y \rightarrow 0$ static
 rod

$F_h = F_B - F_g = \frac{hA}{\cos(\theta)} g \rho_w - \rho_R L A g$

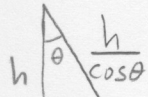
$F_h = A g \left(\frac{\rho_w h}{\cos\theta} - \rho_R L \right)$ downward

another way to write it:
 (3): $F_h = A g \left(\frac{\rho_w h}{\frac{h}{L} \sqrt{\frac{\rho_w}{\rho_R}}} - \rho_R L \right)$
 $= A g L \rho_R \left(\sqrt{\frac{\rho_w}{\rho_R}} - 1 \right)$

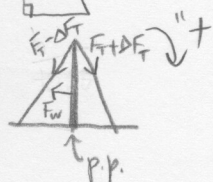
3a.) standing wave in cable w/ lowest resonant frequency f_1



$$f_1 = \frac{v}{\lambda_1} = \frac{\sqrt{F/m}}{2h} \cos\theta$$



b.)



NZL_d:
$$-h(F_T - \Delta F_T) \sin\theta + h(F_T + \Delta F_T) \sin\theta - F_w \frac{h}{2} = I \overset{\text{static}}{\rightarrow} 0$$

$$2 \sin\theta \Delta F_T = \frac{F_w}{2} \quad \Delta F_T = \frac{F_w}{4 \sin\theta}$$

c.)
$$f_{\text{beat}} = |f_1 - f_2| = \frac{\cos\theta}{2h} \left(\sqrt{\frac{F_T + \Delta F_T}{m}} - \sqrt{\frac{F_T - \Delta F_T}{m}} \right)$$

d.) observer is moving w/r to ground but still w/r to the air, which is the medium transmitting the sound waves.

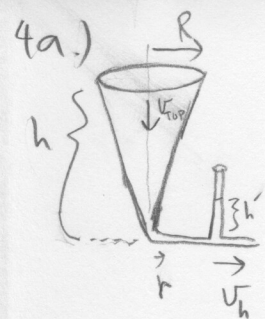
Doppler shift w/ moving source, moving away

$$f_{\text{obs}} = f_B \frac{1}{1 + \frac{u}{v}} \quad \lambda_{\text{obs}} = \frac{v}{f_{\text{obs}}} = \frac{v(1 + \frac{u}{v})}{f_B} = \frac{v+u}{f_B}$$

e.) new observer moving w/r to air: approaching 1st bird

$$f'_{\text{obs}} = f_{\text{obs}} \left(1 + \frac{\text{speed of obs w/r to air}}{v} \right)$$

$$= f_B \frac{1}{1 + \frac{u}{v}} \left(1 + \frac{u' - u}{v} \right)$$



continuous flow through vertical & horizontal pipes
(separate flow in stand pipe)

B.E. $(P + \rho gh + \frac{1}{2} \rho v_{top}^2)_{top} = (P + \rho g 0 + \frac{1}{2} \rho v_{horiz.}^2)_{horiz. pipe}$ (1)

C.E. $A_{top} v_{top} = A_h v_h \Rightarrow v_h = \frac{R^2}{r^2} v_{top}$ (2)

(2) in (1) $\Rightarrow \rho gh + \frac{1}{2} \rho v_{top}^2 = \frac{1}{2} \rho \frac{R^4}{r^4} v_{top}^2$ (3)

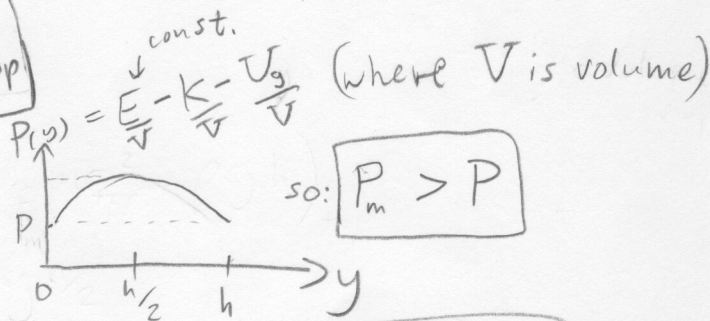
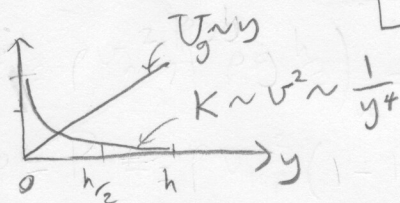
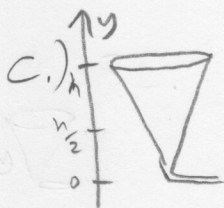
$$R = r \sqrt[4]{\frac{2gh}{v_{top}^2} + 1}$$

since $R \gg r \Rightarrow$ (3): $gh + \frac{1}{2} v_{top}^2 \approx \frac{1}{2} \rho \frac{R^4}{r^4} v_{top}^2$
 $R \approx r \sqrt[4]{\frac{2gh}{v_{top}^2}}$

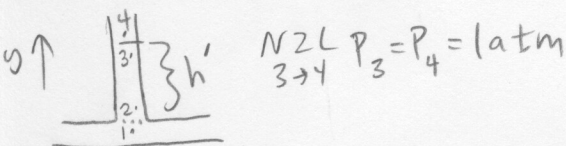
b.) C.E. $A_m v_m = A_t v_{top}$

$$\left(\frac{R+r}{2}\right)^2 v_m = R^2 v_{top}$$

$R \gg r \Rightarrow \frac{R^2}{4} v_m = R^2 v_{top} \Rightarrow v_m = 4 v_{top}$



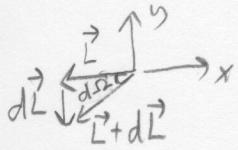
d.) N2L y: $P_1 = P_2$ + B.E: $P_3 + \rho gh' = P_2 \Rightarrow h' = \frac{P_2 - P_3}{\rho g} = \frac{P - 1 \text{ atm}}{\rho g}$



e.) C.E. is unchanged by viscosity: (2): $v_h = \frac{R^2}{r^2} v_{top}$

5a.) $NZL_2: \vec{\tau}_{net} = \frac{d\vec{L}}{dt}$ sphere $I_{cm} = \frac{2}{5}MR^2$ symmetrical about axis of r.
 $\vec{L} = I\vec{\omega}$

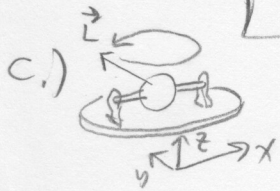
$\omega_2 \ll \omega_1 \Rightarrow \vec{L} = -I_{cm} \omega_1 \hat{i}, \vec{\tau}_{net} = \frac{d\vec{L}}{dt} = L \frac{d\Omega}{dt} (-\hat{j}) = \boxed{-\frac{2}{5}MR^2 \omega_1 \omega_2 \hat{j}}$



$d\vec{L} = L \sin(d\Omega) \hat{j} \approx L d\Omega \hat{j}$

negative y direction

b.) $\vec{L} = I\vec{\omega} = \boxed{\frac{2}{5}MR^2(-\omega_1 \hat{i} + \omega_2 \hat{k})}$



c.) $\vec{\tau}_{net} = \frac{d\vec{L}}{dt} = \text{same as in a) since the x \& y components of } \vec{L} \text{ are the same functions of time as in a) and } L_z \text{ is not changing.}$

$|\vec{\tau}_{net}| = \frac{2}{5}MR^2 \omega_1 \omega_2$

d.) half of this torque is achieved by the force acting on one end of axle:

$\tau_{end} = \frac{l}{2} F = \frac{1}{2} \frac{2}{5} MR^2 \omega_1 \omega_2$

$F = \frac{2}{5} \frac{MR^2 \omega_1 \omega_2}{l}$



density of original sphere = $\rho = \frac{M}{\frac{4}{3}\pi R^3}$

"||" axis thrm: $I = \left(\frac{2}{5}MR^2 + MR^2\right) - \left(\frac{2}{5}mr^2 + m(R-d)^2\right)$

I for solid sphere about end

I for solid sphere about axis d from center

$m = \rho \frac{4}{3}\pi r^3 = M \frac{r^3}{R^3}$

$I = \left(\frac{2}{5}MR^2 + MR^2\right) - \left(\frac{2}{5}M \frac{r^5}{R^3} + M \frac{r^3(R-d)^2}{R^3}\right)$

6a.) $h = \frac{1}{2}H \Rightarrow$ bullet hits c.m. of rack: 1-D problem since no friction or other forces that give torque about pole c.m.

$$|\vec{J}| = J_x = \Delta P_{x, \text{Rack}} = U_{Rf} M_R - \vec{v}_R \cdot M_R$$

\Rightarrow totally inelastic collision:

$$m_B v_B = (m_B + M_R) v_{fR}$$

$$|\vec{J}| = m_B v_B \quad \text{using } m_B \ll M_R$$

b.) $h = \frac{1}{2}H \quad W_{\text{on Rack}} = \Delta K_R = K_{Rf} = \frac{1}{2} M_R v_{fR}^2 = \frac{1}{2} M_R \frac{m_B^2}{M_R^2} v_B^2 = \frac{1}{2} M_B v_B^2 \frac{m_B}{M_R}$

c.) $|\vec{L}| = |\vec{r} \times \vec{p}| = \left(\frac{H}{2} - h\right) m_B v_B$ out of page by R.H.R.

d.) c.o. \vec{L} : $\left(\frac{H}{2} - h\right) m_B v_B = I_{\text{Rack cm}} \omega_{Rf}$ (where we have assumed $m_B \ll M_R$ so c.m. of bullet + Rack = c.m. rack and $L_{Bf} \ll L_{Rf}$)

$$I_{\text{Rack cm}} = 2 \int_0^{H/2} \frac{M_R}{H} dx x^2 = \frac{2 H^3 M_R}{3 \cdot 8 H} = \frac{1}{12} M_R H^2 \quad (2)$$

(2) in (1) $\Rightarrow \quad \frac{H}{2} m_B v_B = \frac{1}{12} M_R H^2 \omega_{Rf}$

$$\omega_{Rf} = \frac{6 m_B v_B}{H M_R}$$

e.) time for Rack to rotate by $\frac{\pi}{2}$: $t_{\text{rotate}} = \frac{\pi/2}{\omega_R} = \frac{\pi H M_R}{12 m_B v_B}$

time for Rack's cm to move by $\frac{H}{2} - D$: $t_{\text{move}} = \frac{\frac{H}{2} - D}{v_{\text{cm}, R}} = \frac{\frac{H}{2} - D}{v_B} \frac{M_R}{m_B}$

c.o. $P_x \quad m_B v_B = (M_R + m_B) v_{Rf, \text{cm}}$

Rack hits D. May be: $t_{\text{rot}} \leq t_{\text{move}}$

$$\frac{\pi H M_R}{12 m_B v_B} \leq \left(\frac{H}{2} - D\right) \frac{1}{v_B} \frac{M_R}{m_B}$$

$$D \leq \frac{H}{2} - \frac{\pi H}{12}$$

$$D \leq \frac{H}{2} \left(1 - \frac{\pi}{6}\right)$$