

**Final Examination**  
**Tuesday May 10, 2016**  
**8:00am to 11:00 am**  
**105 Stanley Hall**

**Closed Books and Closed Notes**  
**For Full Credit Answer Five Questions of your Choice**

**Useful Formulae**

For the corotational bases shown in the figures:

$$\begin{aligned} \mathbf{e}_x &= \cos(\theta)\mathbf{E}_x + \sin(\theta)\mathbf{E}_y, \\ \mathbf{e}_y &= \cos(\theta)\mathbf{E}_y - \sin(\theta)\mathbf{E}_x. \end{aligned} \quad (1)$$

The following identity for the angular momentum of a rigid body relative to a point  $P$  will also be useful:

$$\mathbf{H}_P = \mathbf{H} + (\bar{\mathbf{x}} - \mathbf{x}_P) \times m\bar{\mathbf{v}}. \quad (2)$$

In computing components of moments, the following identity can be useful:

$$(\mathbf{a} \times \mathbf{b}) \cdot \mathbf{E}_z = (\mathbf{E}_z \times \mathbf{a}) \cdot \mathbf{b}, \quad (3)$$

where  $\mathbf{a}$  and  $\mathbf{b}$  are any pair of vectors.

You should also note that

$$|x| = +x \text{ if } x > 0 \text{ and } |x| = -x \text{ if } x < 0. \quad (4)$$

These results are useful when calculating magnitudes.

Finally, recall that the work-energy theorem of a rigid body which is subject to a system of  $K$  forces and a pure moment  $\mathbf{M}_P$  is

$$\dot{T} = \sum_{i=1}^K \mathbf{F}_i \cdot \mathbf{v}_i + \mathbf{M}_P \cdot \boldsymbol{\omega}. \quad (5)$$

Here,  $\mathbf{v}_i$  is the velocity vector of the point  $X_i$  where the force  $\mathbf{F}_i$  is applied and  $\mathbf{M}_P$  is a pure moment.

**Question 1**  
*Motion of a Rigid Rod*  
 (20 Points)

As shown in Figure 1, a thin uniform rod of mass  $m$  and length  $2\ell$  is pin-jointed at  $O$ . One end of a spring of stiffness  $K$  and unstretched length  $\ell_0 = 0$  is attached to a point  $B$  at the apex of the rod. The other end of the spring is attached to a fixed point  $A$ . During the ensuing motion, a vertical gravitational force  $-mg\mathbf{E}_y$  also acts on the rigid body.

The position vectors of the center of mass  $C$  of the rigid body relative to  $O$ , the point  $A$  relative to the point  $O$ , and the point  $B$  relative to  $O$ , and the angular momentum of the rigid body relative to  $C$  have the representations

$$\bar{\mathbf{x}} = \ell\mathbf{e}_x, \quad \mathbf{x}_B = 2\ell\mathbf{e}_x, \quad \mathbf{x}_A = 2\ell\mathbf{E}_y, \quad \mathbf{H} = \left( I_{zz} = \frac{m\ell^2}{3} \right) \dot{\theta}\mathbf{E}_z. \quad (6)$$

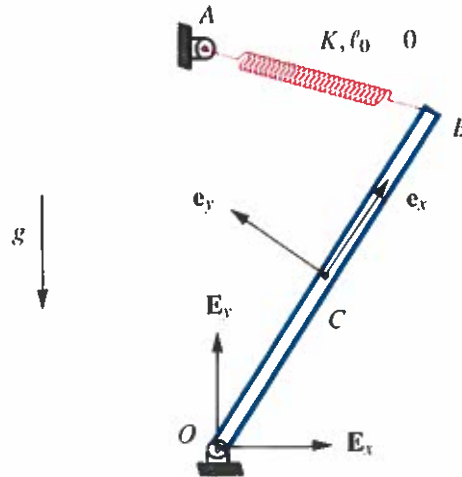


Figure 1: A rigid body of mass  $m$  is free to rotate about  $O$ . The rigid body is subject to a gravitational force and a spring force induced by a spring of stiffness  $K$  and unstretched length  $\ell_0 = 0$ .

- (a) (6 Points) Establish expressions for the angular momentum  $\mathbf{H}_O$  and kinetic energy  $T$  of the rigid body when it is rotating about  $O$ .
- (b) (4 Points) Draw a free-body diagram of the rigid body when it is rotating about  $O$ . For full credit, give clear representations for the forces and moments in this diagram.
- (c) (5 Points) Show that the following differential equation governs  $\theta$  when the body is rotating about  $O$ :

$$\frac{4m\ell^2}{3}\ddot{\theta} = -mg\ell \cos(\theta) + K? \quad (7)$$

For full credit, supply the missing term.

- (d) (5 Points) Starting from the work-energy theorem (5), prove that the total energy  $E$  of the rigid body is conserved. For full credit, supply an expression for the total energy  $E$ .

**Question 2**  
*A Rigid Body on an Incline*  
 (20 Points)

As shown in Figure 2, a long slender rigid rod of mass  $m$ , moment of inertia relative to its center of mass  $C$  of  $I_{zz}$ , and length  $2\ell$ , rests with one end  $A$  on a smooth horizontal surface and the other end  $B$  on a smooth incline. The rod is supported on rigid massless rollers of negligible radii at  $A$  and  $B$ . The position vectors of the points  $A$ ,  $C$ , and  $B$ , have the representations:

$$\begin{aligned} \mathbf{x}_A = x_A \mathbf{E}_x &= -\frac{2\ell}{\sin(\beta)} \sin(\theta + \beta) \mathbf{E}_x, & \bar{\mathbf{x}} = \mathbf{x}_C = \mathbf{x}_A + \ell \mathbf{e}_x, \\ \mathbf{x}_B = s_B (\cos(\beta) \mathbf{E}_x - \sin(\beta) \mathbf{E}_y) &= -\frac{2\ell \sin(\theta)}{\sin(\beta)} (\cos(\beta) \mathbf{E}_x - \sin(\beta) \mathbf{E}_y), \end{aligned} \quad (8)$$

where  $\beta$  is a constant.

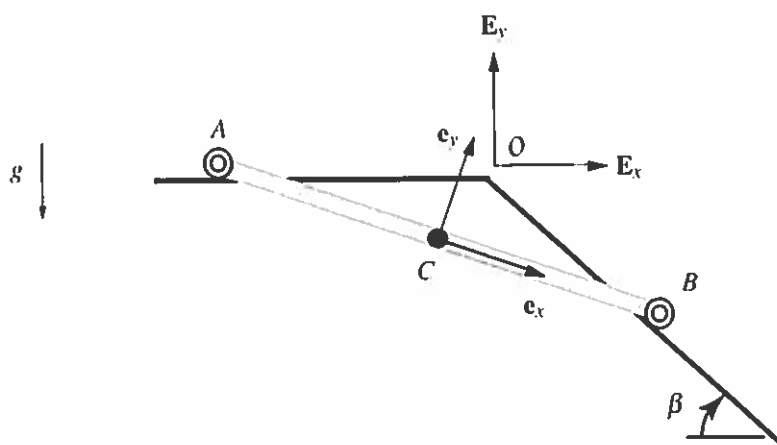


Figure 2: A rigid body of mass  $m$  and length  $2\ell$  is supported at its ends by rigid massless rollers which are free to move on smooth surfaces.

(a) (8 Points) Suppose the body is in motion with  $A$  in contact with the horizontal surface and  $B$  in contact with the incline. Show that the kinetic energy  $T$  and acceleration of the center of mass of the rigid body have the representations

$$\begin{aligned} T &= \frac{\alpha_1}{2} \dot{\theta}^2, \\ \ddot{\mathbf{x}}_C &= -\frac{2\ell}{\sin(\beta)} (\ddot{\theta} \cos(\theta + \beta) - \dot{\theta}^2 \sin(\theta + \beta)) \mathbf{E}_x + \ell \ddot{\theta} \mathbf{e}_y - \ell \dot{\theta}^2 \mathbf{e}_x, \end{aligned} \quad (9)$$

where

$$\alpha_1 = I_{zz} + m\ell^2 \left( 1 + \frac{4\cos^2(\theta + \beta)}{\sin^2(\beta)} + \frac{4\cos(\theta + \beta)\sin(\theta)}{\sin(\beta)} \right). \quad (10)$$

(b) (3 Points) Draw a free-body diagram of the rigid body.

(c) (4 Points) Using the work-energy theorem, prove that the total energy  $E$  of the rigid body is conserved when it is in motion. For full credit, supply an expression for  $E$ .

(d) (5 Points) Using the fact that the total energy is conserved, establish the differential equation governing the motion of the rod. Your solution will be of the form

$$\alpha_1 \ddot{\theta} + \alpha_2 \dot{\theta}^2 + \alpha_3 = 0, \quad (11)$$

where  $\alpha_1$ ,  $\alpha_2$ , and  $\alpha_3$  depend on some of the following parameters and angles:  $I_{zz}$ ,  $m$ ,  $\ell$ ,  $\beta$ ,  $g$ , and  $\theta$ .

**Question 3**  
*A Rolling Rigid Body*  
 (20 Points)

As shown in Figure 3, a rigid body consists of a solid circular axle of radius  $r$  that is connected by a set of webs to a circular wheel of radius  $R$ . The combined body has a mass  $m$  and moment of inertia (relative to its center of mass  $C$ )  $I_{zz}$ . The axle rolls without slipping on a rough inclined rail. The position vector of the center of mass  $C$  has the representation

$$\bar{\mathbf{x}} = x\mathbf{E}_x + r\mathbf{E}_y. \quad (12)$$

A spring of unstretched length  $\ell_0$  and stiffness  $K$  is attached to the point  $C$  on the rigid body and a fixed point  $B$ . The position vector of the point  $B$  is

$$\mathbf{x}_B = r\mathbf{E}_y. \quad (13)$$

Note that in this problem  $x$  takes on negative values.

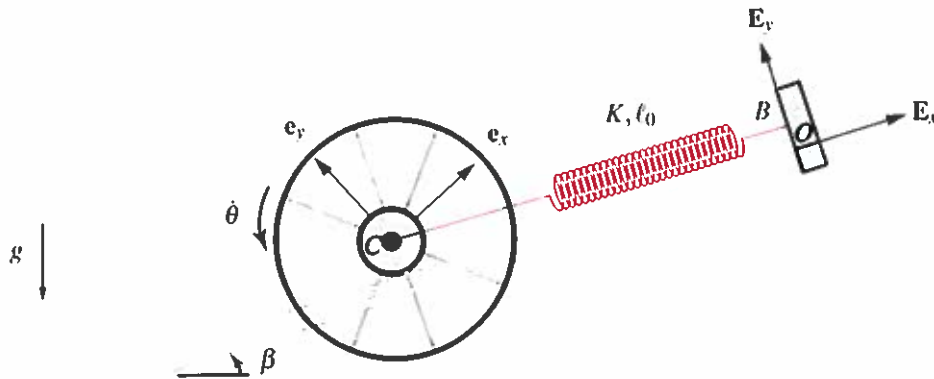


Figure 3: A wheel of mass  $m$  with an axle of radius of  $r$  and an outer radius of  $R$  rolling on an inclined rail.

(a) (4 Points) With the help of the identity  $\mathbf{v}_2 = \mathbf{v}_1 + \boldsymbol{\omega} \times (\mathbf{x}_2 - \mathbf{x}_1)$  applied to two points on the rigid body, show that the slip speed  $v_P$  of the instantaneous point of contact  $P$  of the axle with the inclined rail can be expressed as

$$v_P = \dot{x} + r\dot{\theta}, \quad (14)$$

where  $\boldsymbol{\omega} = \dot{\theta}\mathbf{E}_z$  is the angular velocity of the rigid body.

(b) (5 Points) Draw a free-body diagram of the rigid body. For full credit, give a clear representation for the spring force. You will find it helpful to recall that  $x < 0$  in this problem.

(c) (3+3 Points) Assume that the rigid body is rolling. Using a balance of linear momentum, show that

$$\mathbf{F}_f + \mathbf{N} = m(?? + g(\cos(\beta)\mathbf{E}_y + \sin(\beta)\mathbf{E}_x)) + ??? \quad (15)$$

Show that the equation governing the motion of the rolling body can be expressed as

$$(I_{zz} + ???) \ddot{\theta} = mg???? + K???? \quad (16)$$

For full credit, supply the missing terms in (15) and (16).

(d) (5 Points) Suppose the plane is horizontal ( $\beta = 0$ ) and the rigid body is released from rest at time  $t = 0$  with  $\theta(0) = 0$  and  $x = x_0$ . Establish the range of initial values for  $x_0$  such that the rigid body will roll initially. Your solution should show that this range becomes smaller as the ratio of the gravitational force to the spring stiffness decreases.

**Question 4**  
A Pair of Rigid Bodies (20 Points)

As shown in Figure 4, a uniform thin rod of mass  $m_1$ , moment of inertia about  $O$  of  $I_{Oz}$ , and length  $\ell$  is free to rotate about a fixed point  $O$ . At the end of the rod, a rod of mass  $m_2$ , length  $2R$  and moment of inertia  $I_{Cz} = \frac{1}{3}m_2R^2$  about its center of mass  $C_2$  is attached by a pin joint and is free to rotate about  $\mathbf{E}_z$ .

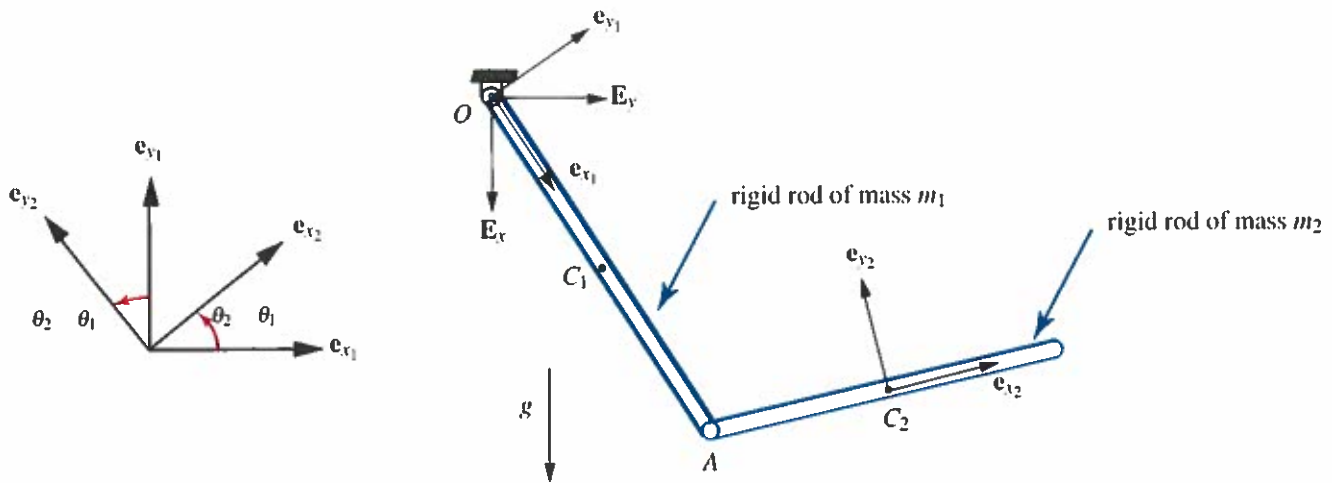


Figure 4: A uniform rod of length  $\ell$  and mass  $m_1$  is free to rotate about a fixed point  $O$ . At the other end of the rod, a rod of mass  $m_2$  and length  $2R$  is free to rotate about the  $\mathbf{E}_z$  axis. The sketch of the corotational bases on the left facilitates computing their cross products and inner products.

Relative to a fixed origin  $O$ , the center of mass  $C_1$  of the rod of length  $\ell$  and the point  $C_2$  have the following position vectors:

$$\bar{\mathbf{x}}_1 = \frac{\ell}{2}\mathbf{e}_{x_1}, \quad \bar{\mathbf{x}}_2 = \ell\mathbf{e}_{x_1} + R\mathbf{e}_{x_2}, \quad (17)$$

where

$$\mathbf{e}_{x_\alpha} = \cos(\theta_\alpha)\mathbf{E}_x + \sin(\theta_\alpha)\mathbf{E}_y, \quad \mathbf{e}_{y_\alpha} = -\sin(\theta_\alpha)\mathbf{E}_x + \cos(\theta_\alpha)\mathbf{E}_y, \quad \alpha = 1, 2. \quad (18)$$

The angular momentum of the rod of length  $2R$  relative to its center of mass  $C_2$  is

$$\mathbf{H}_{\text{rod}_2} = \frac{1}{3}m_2R^2\dot{\theta}_2\mathbf{E}_z, \quad (19)$$

where  $\dot{\theta}_2\mathbf{E}_z$  is the angular velocity of the rod of length  $2R$ .

(a) (5 Points) Show that the linear momentum  $\mathbf{G}$  of the system has the representation

$$\mathbf{G} = \left(m_1\frac{\ell}{2} + m_2\ell\right)\dot{\theta}_1\mathbf{e}_{y_1} + m_2R\dot{\theta}_2\mathbf{e}_{y_2}. \quad (20)$$

(b) (7 Points) Show that the angular momentum  $\mathbf{H}_O$  of the system relative to  $O$  is

$$\mathbf{H}_O = (I_{Oz} + m_2\ell^2)\dot{\theta}_1\mathbf{E}_z + \frac{4}{3}m_2R^2\dot{\theta}_2\mathbf{E}_z + ??\dot{\theta}_1\mathbf{E}_z + ???\dot{\theta}_2\mathbf{E}_z. \quad (21)$$

For full credit supply the missing terms.

(c) (8 Points) Show that the kinetic energy  $T$  of the system has the representation

$$T = a_1\dot{\theta}_1^2 + a_2\dot{\theta}_2^2 + a_3\dot{\theta}_1\dot{\theta}_2. \quad (22)$$

For full credit, supply expressions for the coefficients  $a_1$ ,  $a_2$ , and  $a_3$ . These coefficients will depend on the parameters of the system and may also depend on the angles  $\theta_1$  and  $\theta_2$ .

### Question 5

*A Collar on a Rotating Rod (20 Points)*

As shown in Figure 5, a uniform thin rod of mass  $m_1$ , moment of inertia about  $O$  of  $I_{O_{zz}}$ , and length  $\ell$  is free to rotate about a fixed point  $O$ . A collar of mass  $m_2$  is attached to the end of the rod by a spring of unstretched length  $\ell_0$  and stiffness  $K$ . Vertical gravitational forces in the  $\mathbf{E}_z$  direction act on the system and an applied moment  $M_a \mathbf{E}_z$  acts on the rod.

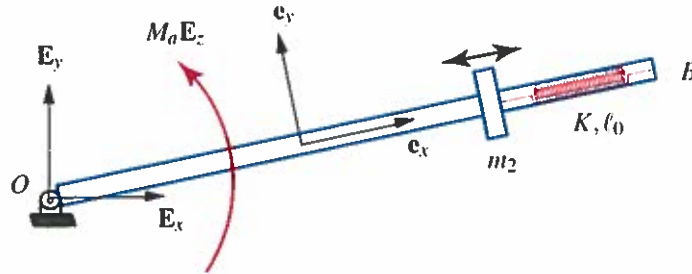


Figure 5: A uniform rod of length  $\ell$  and mass  $m_1$  is free to rotate about a fixed point  $O$  and a collar of mass  $m_2$  is attached by a spring to a point  $B$  at the end of the rod. The collar is free to move on the smooth rod. Vertical gravitational forces  $-m_1 g \mathbf{E}_z$  and  $-m_2 g \mathbf{E}_z$  act on system.

Relative to a fixed origin  $O$ , the center of mass  $C$  of the rod of length  $\ell$  and the collar have the following position vectors:

$$\bar{\mathbf{x}} = \frac{\ell}{2} \mathbf{e}_x, \quad \mathbf{r} = r \mathbf{e}_x. \quad (23)$$

(a) (5 Points) Show that the linear momentum  $\mathbf{G}$  of the system has the representation

$$\mathbf{G} = \left( m_1 \frac{\ell}{2} + m_2 r \right) \dot{\theta} \mathbf{e}_y + m_2 \dot{r} \mathbf{e}_x. \quad (24)$$

Show that the angular momentum of the system relative to  $O$  is

$$\mathbf{H}_O = (I_{O_{zz}} + m_2 r^2) \dot{\theta} \mathbf{E}_z. \quad (25)$$

(b) (5 Points) Draw freebody diagrams of (i) the collar of mass  $m_2$ , and (ii) the collar-rod system.

(c) (5 Points) Show that the motion of the collar is governed by the differential equation

$$m_2 (\ddot{r} - r \dot{\theta}^2) + K? = 0. \quad (26)$$

For full credit supply the missing term.

(d) (5 Points) Show that the angle of rotation  $\theta$  is governed by the differential equation

$$b_1 \ddot{\theta} + b_2 \dot{\theta} + b_3 = 0. \quad (27)$$

For full credit, supply expressions for the coefficients  $b_1$ ,  $b_2$ , and  $b_3$  in terms of the parameters  $I_{O_{zz}}$ ,  $m_2$ , applied moment  $M_a$ , and displacement  $r$ .

### Question 6

*A Block Colliding with a Fixed Point (20 Points)*

As shown in Figure 6, a uniform rigid block of mass  $m$ , height  $h$ , width  $w$  and moment of inertia  $I_{zz}$  traveling with a velocity  $v_0 \mathbf{E}_y$  and rotating with an angular velocity  $\boldsymbol{\omega} = \omega_0 \mathbf{E}_z$  collides with an obstacle at  $O$ . After the impact, the rigid body rotates about one of its corner points that remains in contact with  $O$ .

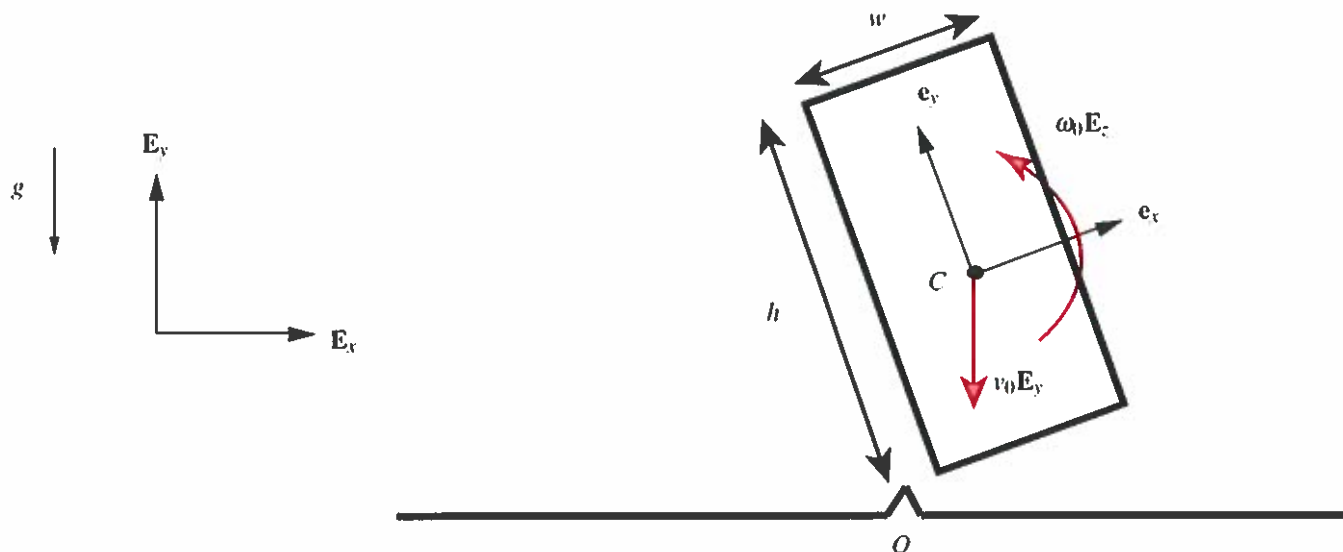


Figure 6: A rigid body of mass  $m$  collides with a rigid obstacle at  $O$  with  $v_0 < 0$  and  $\omega_0 > 0$ . After the impact, the rigid body is assumed to rotate about  $O$ .

(a) (5 Points) Using the following representation for the position vector of the center of mass  $C$  relative to  $O$  at the instant just prior to the impact,

$$\bar{\mathbf{x}} - \mathbf{x}_O = \frac{1}{2} (w (\cos(\theta_0) \mathbf{E}_x + \sin(\theta_0) \mathbf{E}_y) + h (\cos(\theta_0) \mathbf{E}_y - \sin(\theta_0) \mathbf{E}_x)), \quad (28)$$

establish expressions for the angular momentum  $\mathbf{H}_O$ , kinetic energy  $T$ , and total energy  $E$  of the rigid body at the instant just before the collision.

(b) (5 Points) Starting from the following representation for the position vector of the center of mass  $C$  relative to  $O$ ,

$$\bar{\mathbf{x}} - \mathbf{x}_O = \frac{1}{2} (w \mathbf{e}_x + h \mathbf{e}_y), \quad (29)$$

establish expressions for the angular momentum  $\mathbf{H}_O$ , kinetic energy  $T$ , and total energy  $E$  of the rigid body at any instant following the collision.

(c) (5 Points) Show that the angular velocity of the rigid body at the instant immediately following the collision is

$$\boldsymbol{\omega} = \frac{mv_0 (w \cos(\theta_0) - h \sin(\theta_0)) + 2I_{zz} \omega_0}{2 \left( I_{zz} + \frac{m}{4} (h^2 + w^2) \right)} \mathbf{E}_z. \quad (30)$$

(d) (5 Points) Suppose that  $\omega_0 = 0$  (i.e., the rigid body is not rotating prior to the collision). With the help of (30), show that the energy loss due to the collision is proportional to  $\frac{m}{2} v_0^2$  and that the impulse of the reaction force at  $O$  during the collision is proportional to  $mv_0$ .

QUESTION 1

(a)

$$\underline{\underline{x}} = l \underline{\underline{e}}_x \Rightarrow \underline{\underline{v}} = l \dot{\theta} \underline{\underline{e}}_y$$

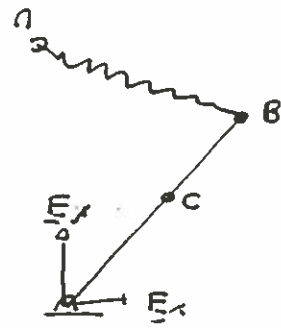
$$\underline{\underline{H}}_0 = \underline{\underline{H}} + \underline{\underline{x}} \times m \underline{\underline{v}}$$

$$= \frac{m \omega^2}{3} \dot{\theta} \underline{\underline{e}}_z + l \underline{\underline{e}}_x \times m l \dot{\theta} \underline{\underline{e}}_y$$

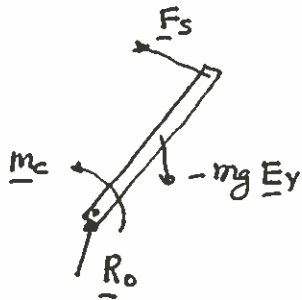
$$= \left( \frac{m \omega^2}{3} + m \omega^2 \right) \dot{\theta} \underline{\underline{e}}_z = \frac{4 m \omega^2}{3} \dot{\theta} \underline{\underline{e}}_z$$

$$T = \frac{1}{2} m \underline{\underline{v}} \cdot \underline{\underline{v}} + \frac{1}{2} \underline{\underline{H}} \cdot \underline{\underline{\omega}}$$

$$= \frac{1}{2} m l^2 \dot{\theta}^2 + \frac{1}{2} \left( \frac{4 m \omega^2}{3} \right) \dot{\theta}^2 = \frac{1}{2} \left( \frac{4 m l^2}{3} \right) \dot{\theta}^2$$



(b)



$$\underline{\underline{F}}_s = -K (\| \underline{\underline{x}}_B - \underline{\underline{x}}_A \| - 0) \frac{\underline{\underline{x}}_B - \underline{\underline{x}}_A}{\| \underline{\underline{x}}_B - \underline{\underline{x}}_A \|}$$

$$= -K (\underline{\underline{x}}_B - \underline{\underline{x}}_A)$$

$$= -K(2l)(\underline{\underline{e}}_x - \underline{\underline{e}}_y)$$

(c)  $(\underline{\underline{M}}_0 = \underline{\underline{H}}_0) \cdot \underline{\underline{e}}_z$

$$\frac{4 m l^2}{3} \ddot{\theta} = (l \underline{\underline{e}}_x \times -mg \underline{\underline{e}}_y) \cdot \underline{\underline{e}}_z + (2l \underline{\underline{e}}_x \times \underline{\underline{F}}_s) \cdot \underline{\underline{e}}_z$$

$$= -mg \underline{\underline{e}}_x \cdot l \underline{\underline{e}}_x + 2l \underline{\underline{e}}_y \cdot \underline{\underline{F}}_s$$

$$= -mg l \cos \theta + 4 K l^2 \cos \theta$$

(d)  $\dot{T} = \underline{\underline{R}}_0 \cdot \underline{\underline{v}}_0 + \underline{\underline{m}}_c \cdot \underline{\underline{\omega}} - mg \underline{\underline{e}}_y \cdot \underline{\underline{v}} + \underline{\underline{F}}_s \cdot \underline{\underline{v}}_B$

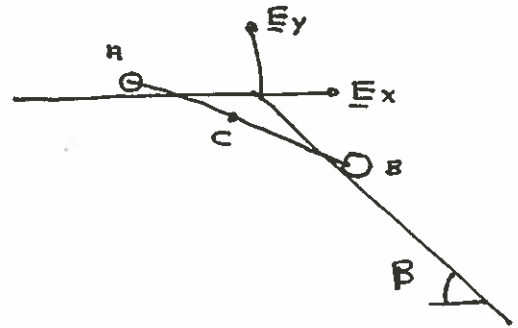
$$= 0 + 0 - \frac{d}{dt} (mg \underline{\underline{e}}_y \cdot \underline{\underline{x}} + \frac{1}{2} K (\| \underline{\underline{x}}_B - \underline{\underline{x}}_A \|^2))$$

$$\Rightarrow \frac{d}{dt} (E = T + mg \underline{\underline{e}}_y \cdot \underline{\underline{x}} + \frac{1}{2} K (\| \underline{\underline{x}}_B - \underline{\underline{x}}_A \|^2)) = 0$$

$\Rightarrow E$  is conserved.



QUESTION 2



$$\underline{x}_A = \underline{x}_A \underline{E}_x = -\frac{2l}{\sin\beta} \sin(\theta+\beta) \underline{E}_x$$

$$\underline{\tilde{x}} = \underline{x}_A + l \underline{E}_x$$

$$\underline{x}_B = S_B (\cos\beta \underline{E}_x - \sin\beta \underline{E}_y) \quad S_B = -\frac{2l \sin\theta}{\sin\beta}$$

(a) 
$$\underline{\tilde{v}} = \underline{v}_A + l \dot{\theta} \underline{E}_x = -\frac{2l \dot{\theta}}{\sin\beta} \cos(\theta+\beta) \underline{E}_x + l \dot{\theta} \underline{E}_y$$

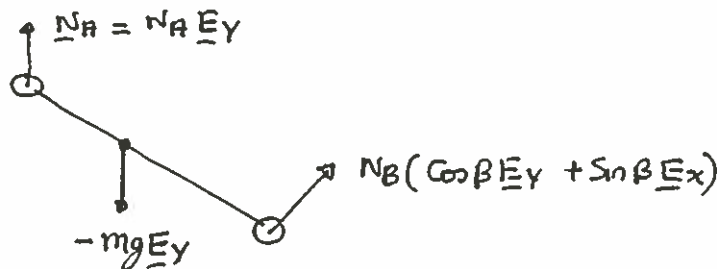
$$\underline{\tilde{a}} = l \ddot{\theta} \underline{E}_y - l \dot{\theta}^2 \underline{E}_x + \frac{2l \dot{\theta}^2 \sin(\theta+\beta)}{\sin\beta} \underline{E}_x - \frac{2l \ddot{\theta}}{\sin\beta} \cos(\theta+\beta) \underline{E}_x$$

$$T = \frac{1}{2} m \underline{\tilde{v}} \cdot \underline{\tilde{v}} + \frac{1}{2} I_{zz} \dot{\theta}^2$$

$$= \frac{1}{2} m \left( l^2 \dot{\theta}^2 + \frac{4l^2 \dot{\theta}^2}{\sin^2\beta} \cos^2(\theta+\beta) + \frac{4l^2 \dot{\theta}^2}{\sin\beta} \cos(\theta+\beta) \sin\theta \right)$$

$$+ \frac{1}{2} I_{zz} \dot{\theta}^2$$

(b)



(c) 
$$\dot{T} = \underline{N}_A \cdot \underline{v}_A + \underline{N}_B \cdot \underline{v}_B - mg \underline{E}_y \cdot \underline{\tilde{v}}$$

$$\underline{N}_A \cdot \underline{v}_A = 0 \quad \because \underline{N}_A \perp \underline{v}_A$$

$$\underline{N}_B \cdot \underline{v}_B = 0 \quad \because \underline{N}_B \perp \underline{v}_B$$

$$= -\frac{d}{dt} (mg \underline{E}_y \cdot \underline{\tilde{x}})$$

$$\Rightarrow \frac{d}{dt} (E = T + mg \underline{E}_y \cdot \underline{\tilde{x}}) = 0 \Rightarrow E \text{ is conserved.}$$

where  $mg \underline{E}_y \cdot \underline{\tilde{x}} = mgl \sin\theta$

(d) E is conserved

$$E = T + mg \underline{E}_y \cdot \underline{\hat{x}}$$

$$= T + mgL \sin \theta$$

$$\dot{E} = 0 \Rightarrow \dot{T} + mgL \dot{\theta} \cos \theta = 0$$

$$\text{Now } \dot{T} = \left( I_{zz} + mL^2 \left( 1 + \frac{4 \cos^2(\theta + \beta)}{\sin^2 \beta} + \frac{4 \cos(\theta + \beta) \sin \theta}{\sin \beta} \right) \right) \ddot{\theta} \dot{\theta}$$

$$+ \frac{mL^2}{\sin^2 \beta} \left( -4 \cos(\theta + \beta) \sin(\theta + \beta) \right) \dot{\theta}^3$$

$$+ \frac{mL^2}{\sin \beta} \left( -2 \sin(\theta + \beta) \sin \theta + 2 \cos(\theta + \beta) \cos \theta \right) \dot{\theta}^3$$

So we find an equation of the form

$$(\alpha_1 \ddot{\theta} + \alpha_2 \dot{\theta}^2 + \alpha_3) \dot{\theta} = 0 \Leftrightarrow \dot{E} = 0$$

This equation must hold for all  $\dot{\theta}$  so,

$$\alpha_1 \ddot{\theta} + \alpha_2 \dot{\theta}^2 + \alpha_3 = 0$$

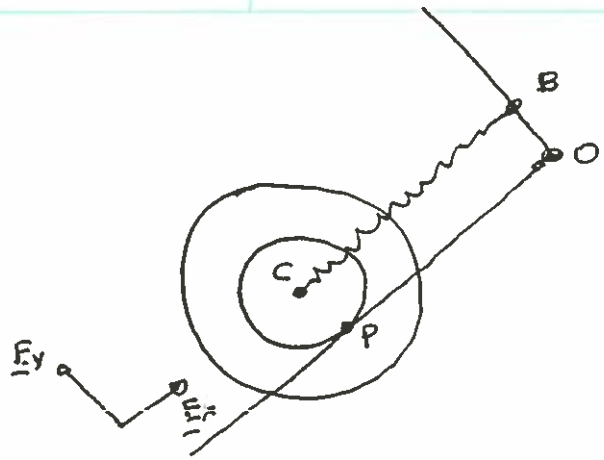
where

$$\alpha_3 = mgL \cos \theta$$

$$\alpha_2 = + \frac{mL^2}{\sin \beta} \left( \begin{array}{l} 2 \cos(\theta + \beta) \cos \theta - 2 \sin(\theta + \beta) \sin \theta \\ - \frac{4 \cos(\theta + \beta) \sin(\theta + \beta)}{\sin \beta} \end{array} \right)$$

$$\alpha_1 = I_{zz} + mL^2 \left( 1 + \frac{4 \cos^2(\theta + \beta)}{\sin^2 \beta} + \frac{4 \cos(\theta + \beta) \sin \theta}{\sin \beta} \right)$$

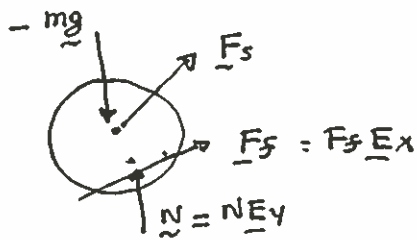
QUESTION 3



$$\begin{aligned}
 \underline{v}_P &= \underline{\dot{y}} + \underline{\omega} \times (\underline{x}_P - \underline{x}) \\
 &= \dot{x} \underline{E}_x + \dot{\theta} \underline{E}_z \times (-r \underline{E}_y) \\
 &= (\dot{x} + r\dot{\theta}) \underline{E}_x
 \end{aligned}$$

Hence  $v_P = \dot{x} + r\dot{\theta} = \underline{v}_P \cdot \underline{E}_x$

(b)



$$\underline{g} = (\cos\beta \underline{E}_y + \sin\beta \underline{E}_x) g$$

$$\underline{F}_s = -K \epsilon \frac{\underline{x} - \underline{x}_B}{\|\underline{x} - \underline{x}_B\|}$$

$$\epsilon = \|\underline{x} - \underline{x}_B\| - l_0$$

$$\|\underline{x} - \underline{x}_B\| = -x \quad \text{as } x < 0$$

$$\underline{F}_s = +K(-x - l_0) \underline{E}_x$$

(c)

$$\underline{F} = m \underline{\ddot{a}} : \quad \underline{F}_s + \underline{F}_f + \underline{N} - m \underline{g} = m \underline{\ddot{x}} \underline{E}_x$$

Hence

$$F_f = m \ddot{x} - K(-x - l_0) + mg \sin\beta$$

$$N = mg \cos\beta$$

$$(\underline{M} = \underline{I} \dot{\underline{H}}) \cdot \underline{E}_z$$

$$I_{zz} \ddot{\theta} = r F_f$$

Substituting for  $F_f$  from  $\underline{F} = m\bar{a}$  and using the condition  $\ddot{x} = -r\ddot{\theta}$  we find that

$$I_{zz}\ddot{\theta} = r(-mr\ddot{\theta} - K(-x-l_0) + mg\delta \sin\beta)$$

Hence  $(I_{zz} + mr^2)\ddot{\theta} = Kr(x+l_0) + mgr\sin\beta$

(d) Initially  $\theta = \theta_0$ ,  $x = x_0$ ,  $\dot{\theta} = 0$ ,  $\dot{x} = 0$ ,

Hence

$$\begin{aligned} F_f &= \frac{1}{r} I_{zz} \ddot{\theta}_0 \\ &= \frac{\frac{1}{r} I_{zz}}{I_{zz} + mr^2} (Kr(x_0 + l_0) + mgr\sin\beta) \end{aligned}$$

Static Friction Criterion

$$|F_f| \leq \mu_s |N| \quad \text{where } N = mg \cos\beta$$

For the case of hard  $\beta = 0$ , so criterion simplifies to.

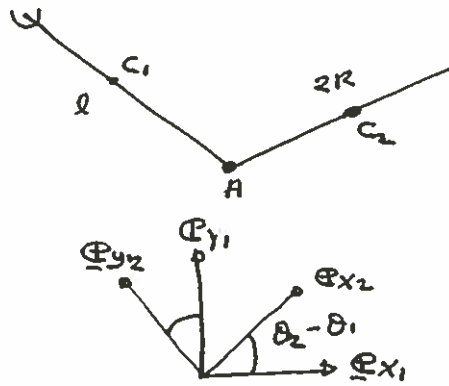
$$\frac{I_{zz} K}{I_{zz} + mr^2} |x_0 + l_0| \leq \mu_s mg$$

Hence

$$|x_0 + l_0| \leq \mu_s \left( \frac{mg}{K} \right) \frac{I_{zz} + mr^2}{I_{zz}}$$

if rolling is to occur. The range is linearly proportional to the ratio  $\frac{mg}{K}$ .

QUESTION 4



$$\begin{aligned}
 \underline{G} &= m_1 \underline{\bar{v}}_1 + m_2 \underline{\bar{v}}_2 \\
 &= m_1 \underline{\dot{x}}_1 + m_2 \underline{\dot{x}}_2 \\
 &= m_1 \frac{l}{2} \dot{\theta} \underline{e}_{y1} + m_2 l \dot{\theta} \underline{e}_{y1} + m_2 R \dot{\theta}_2 \underline{e}_{y2} \\
 &= \left( \frac{m_1 l}{2} + m_2 l \right) \dot{\theta} \underline{e}_{y1} + m_2 R \dot{\theta}_2 \underline{e}_{y2}
 \end{aligned}$$

$$\begin{aligned}
 \underline{H}_O &= \underline{H}_O^1 + \underline{H}_O^2 \\
 &= I_{O22} \dot{\theta}_1 \underline{E}_z + \underline{H}_O^2 \\
 &= I_{O22} \dot{\theta}_1 \underline{E}_z + \frac{1}{3} m_2 R^2 \dot{\theta}_2 \underline{E}_z + (\underline{x}_2) \times m_2 \underline{\bar{v}}_2
 \end{aligned}$$

Now

$$\begin{aligned}
 \underline{x}_2 \times m_2 \underline{\bar{v}}_2 &= (l \underline{e}_{x1} + R \underline{e}_{x2}) \times (m_2 l \dot{\theta}_1 \underline{e}_{y1} + m_2 R \dot{\theta}_2 \underline{e}_{y2}) \\
 &= m_2 l^2 \dot{\theta}_1 \underline{E}_z + m_2 R^2 \dot{\theta}_2 \underline{E}_z \\
 &\quad + (m_2 l R \dot{\theta}_1 \cos(\theta_2 - \theta_1) + m_2 R l \dot{\theta}_2 \cos(\theta_2 - \theta_1)) \underline{E}_z
 \end{aligned}$$

$$\begin{aligned}
 \underline{H}_O &= (I_{O22} + m_2 l^2) \dot{\theta}_1 \underline{E}_z + \frac{4}{3} m_2 R^2 \dot{\theta}_2 \underline{E}_z \\
 &\quad + (m_2 l \dot{\theta}_1 + m_2 l \dot{\theta}_2) (l R \cos(\theta_2 - \theta_1)) \underline{E}_z
 \end{aligned}$$

$$(c) \quad T = \frac{1}{2} m_1 \underline{\dot{v}}_1 \cdot \underline{\dot{v}}_1 + \frac{1}{2} \underline{H}_1 \cdot \dot{\theta}_1 \underline{E}_z \\ + \frac{1}{2} m_L \underline{\dot{v}}_L \cdot \underline{\dot{v}}_L + \frac{1}{2} \underline{H}_L \cdot \dot{\theta}_L \underline{E}_z$$

$$\frac{1}{2} m_1 \underline{\dot{v}}_1 \cdot \underline{\dot{v}}_1 + \frac{1}{2} \underline{H}_1 \cdot \dot{\theta}_1 \underline{E}_z = \frac{1}{2} \underline{H}_{O_1} \cdot \dot{\theta}_1 \underline{E}_z = \frac{1}{2} I_{O_2L} \dot{\theta}_1^2$$

$$\frac{1}{2} \underline{H}_L \cdot \dot{\theta}_L \underline{E}_z = \frac{1}{6} m_2 R^2 \dot{\theta}_2^2$$

$$\frac{1}{2} m_L \underline{\dot{v}}_L \cdot \underline{\dot{v}}_L = \frac{1}{2} m_L (l \dot{\theta}_1 \underline{e}_{y_1} + R \dot{\theta}_2 \underline{e}_{y_2}) \cdot (l \dot{\theta}_1 \underline{e}_{y_1} + R \dot{\theta}_2 \underline{e}_{y_2}) \\ = \frac{1}{2} m_L (l^2 \dot{\theta}_1^2 + R^2 \dot{\theta}_2^2 + 2lR \dot{\theta}_1 \dot{\theta}_2 \underline{e}_{y_1} \cdot \underline{e}_{y_2}) \\ = \frac{1}{2} m_L (l^2 \dot{\theta}_1^2 + R^2 \dot{\theta}_2^2 + 2lR \dot{\theta}_1 \dot{\theta}_2 \cos(\theta_2 - \theta_1))$$

Combining terms

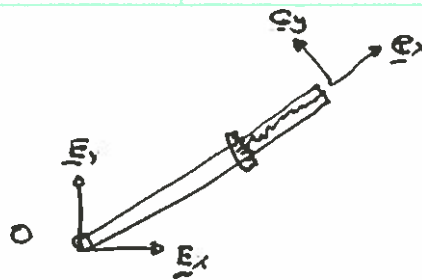
$$T = a_1 \dot{\theta}_1^2 + a_2 \dot{\theta}_2^2 + a_3 \dot{\theta}_1 \dot{\theta}_2$$

$$a_1 = \frac{1}{2} I_{O_2L} + \frac{m_L l^2}{2}$$

$$a_2 = \frac{1}{6} m_L R^2 + \frac{1}{2} m_2 R^2$$

$$a_3 = m_L l R \dot{\theta}_1 \dot{\theta}_2 \cos(\theta_2 - \theta_1)$$

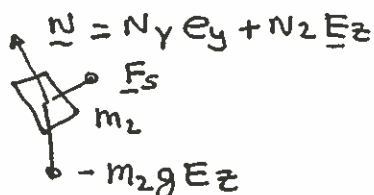
QUESTION 5



$$\begin{aligned} \underline{G} &= m_1 \underline{\dot{x}} + m_2 \underline{\dot{r}} \\ &= m_1 \frac{l}{2} \dot{\theta} \underline{e}_y + m_2 (\dot{r} \underline{e}_x + r \dot{\theta} \underline{e}_y) \\ &= \left( \frac{m_1 l}{2} + m_2 r \right) \dot{\theta} \underline{e}_y + m_2 \dot{r} \underline{e}_x \end{aligned}$$

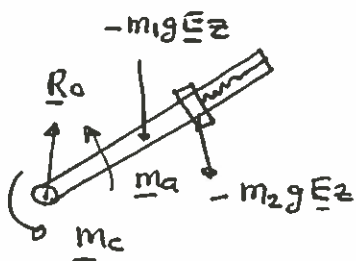
$$\begin{aligned} \underline{H}_O &= I_{O22} \dot{\theta} \underline{e}_z + \underline{r} \times m \underline{v} \\ &= I_{O22} \dot{\theta} \underline{e}_z + m_2 r^2 \dot{\theta} \underline{e}_z \\ &= (I_{O22} + m_2 r^2) \dot{\theta} \underline{e}_z \end{aligned}$$

(b)



$$\underline{F}_s = -K(\varepsilon) \frac{r - l \underline{e}_x}{\|r - l \underline{e}_x\|}$$

$$\begin{aligned} \varepsilon &= |r - l| - l_0 \\ &= l - r - l_0 \end{aligned}$$



$$\underline{m}_c = m_{cx} \underline{e}_x + m_{cy} \underline{e}_y$$

$$(c) \quad \underline{F} = m_2 \underline{\ddot{r}} \Rightarrow \underline{N} + \underline{F}_s - m_2 g \underline{e}_z = m_2 ((\ddot{r} - r \dot{\theta}^2) \underline{e}_x + (r \ddot{\theta} + 2\dot{r} \dot{\theta}) \underline{e}_y)$$

$$\cdot \underline{e}_x \quad m_2 (\ddot{r} - r \dot{\theta}^2) = \underline{F}_s \cdot \underline{e}_x$$

$$\underline{F}_s \cdot \underline{e}_x = -K(l - r - l_0) \frac{r - l}{|r - l|} = K(l - r - l_0)$$

Hence

$$m_2(\ddot{r} - r\dot{\theta}^2) = k(l - r - l_0).$$

(d)  $\underline{M}_0 = \underline{H}_0$  for system

$$\underline{H}_0 = (I_{O_{22}} + m_2 r^2) \ddot{\theta} \underline{E}_z + 2m_2 r \dot{r} \dot{\theta} \underline{E}_z$$

$$\underline{M}_0 \cdot \underline{E}_z = Ma$$

Hence

$$(I_{O_{22}} + m_2 r^2) \ddot{\theta} + 2m_2 r \dot{r} \dot{\theta} = Ma.$$

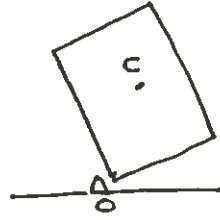
$$\Rightarrow b_1 = I_{O_{22}} + m_2 r^2$$

$$b_2 = 2m_2 r \dot{r}$$

$$b_3 = -Ma$$



## QUESTION 6



(a)

$$\underline{\bar{x}} - \underline{x}_0 = \frac{w}{2} \underline{e}_x (\theta = \theta_0) + \frac{h}{2} \underline{e}_y (\theta = \theta_0)$$

$$\underline{\bar{v}} = v_0 \underline{e}_y$$

$$\underline{H} = I_{zz} \dot{\theta} \underline{e}_z = I_{zz} \omega_0 \underline{e}_z$$

$$\begin{aligned} \underline{H}_0 &= \underline{H} + (\underline{\bar{x}} - \underline{x}_0) \times m \underline{\bar{v}} \\ &= I_{zz} \omega_0 \underline{e}_z + \frac{m}{2} v_0 \left( w \cos \theta_0 - h \sin \theta_0 \right) \underline{e}_z \end{aligned}$$

$$\begin{aligned} T &= \frac{1}{2} m \underline{\bar{v}} \cdot \underline{\bar{v}} + \frac{1}{2} \underline{H} \cdot \underline{\omega} \\ &= \frac{1}{2} m v_0^2 + \frac{1}{2} I_{zz} \omega_0^2 \end{aligned}$$

$$\begin{aligned} E &= T + mg \underline{e}_y \cdot \underline{\bar{x}} \\ &= T + mg \left( \frac{w}{2} \sin \theta_0 + \frac{h}{2} \cos \theta_0 \right) \end{aligned}$$

(b)  $\underline{\bar{x}} - \underline{x}_0 = \frac{1}{2} (w \underline{e}_x + h \underline{e}_y)$

$$\underline{\bar{v}} = \frac{\dot{\theta}}{2} (w \underline{e}_y - h \underline{e}_x)$$

$$T = \frac{1}{2} I_{ozz} \dot{\theta}^2 = \frac{1}{2} \left( I_{zz} + \frac{m}{4} h^2 + \frac{m}{4} w^2 \right) \dot{\theta}^2$$

$$\underline{H}_0 = I_{ozz} \dot{\theta} \underline{e}_z = \left( I_{zz} + \frac{m}{4} h^2 + \frac{m}{4} w^2 \right) \dot{\theta} \underline{e}_z$$

$$E = \frac{1}{2} I_{ozz} \dot{\theta}^2 + mg \left( \frac{w}{2} \sin \theta + \frac{h}{2} \cos \theta \right)$$

(c)  $H_0$  is conserved during collision

$$I_{O22} \dot{\theta} \underline{E}_z = \left( I_{O22} \omega_0 + \frac{m}{2} v_0 (\omega_0 \cos \theta_0 - h \sin \theta_0) \right) \underline{E}_z$$

So,

$$\underline{\omega} = \dot{\theta} \underline{E}_z = \frac{2 I_{O22} \omega_0 + m v_0 (\omega_0 \cos \theta_0 - h \sin \theta_0)}{2 I_{O22}} \underline{E}_z$$

(d) No rotation prior to impact hence

$$\underline{\omega} = \frac{m (\omega_0 \cos \theta_0 - h \sin \theta_0)}{2 I_{O22}} v_0 \underline{E}_z = \Gamma v_0 \underline{E}_z$$

Change in energy during collision is purely kinetic.

$$\begin{aligned} \Delta T &= \frac{1}{2} I_{O22} \left( \frac{m^2 (\omega_0 \cos \theta_0 - h \sin \theta_0)^2}{4 I_{O22}^2} \right) v_0^2 - \frac{1}{2} m v_0^2 \\ &= \frac{1}{2} m v_0^2 \left( -1 + \frac{m (\omega_0 \cos \theta_0 - h \sin \theta_0)^2}{4 I_{O22}} \right) \end{aligned}$$

So  $\Delta T$  is proportional to  $\frac{1}{2} m v_0^2$

$$\text{Impulse of } \underline{R}_0 = \underline{G}_{\text{after}} - \underline{G}_{\text{before}} = \Delta \underline{G}$$

$$= m \Gamma v_0 \left( \omega_0 \underline{e}_y (\theta = \theta_0) + h \underline{e}_x (\theta = \theta_0) \right) - m v_0 \underline{E}_y$$

$$= m v_0 \left( -\underline{E}_y + \Gamma \omega_0 \underline{e}_y (\theta = \theta_0) - \Gamma h \underline{e}_x (\theta = \theta_0) \right)$$

Hence impulse is proportional to  $m v_0$ .