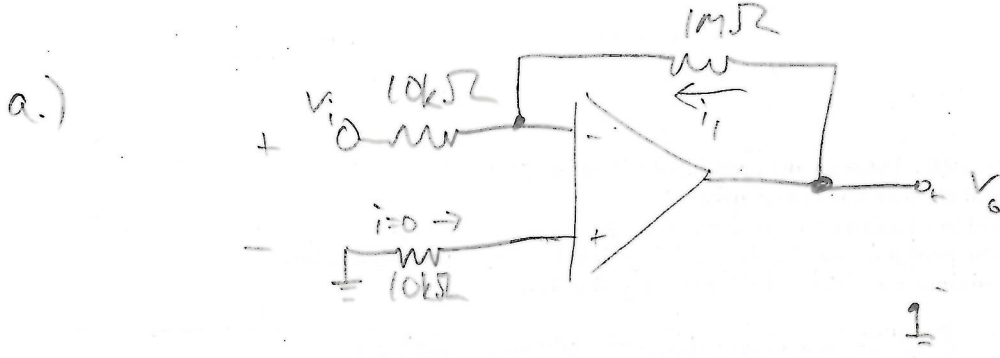
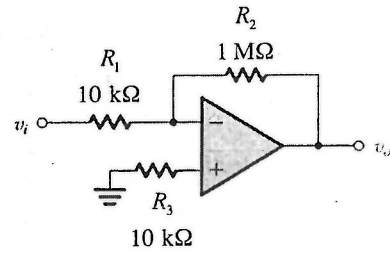


1. Consider the Op Amp circuit on the right.

a. Derive the voltage gain expression of the amplifier if we consider the Op Amp to be ideal (infinite open-loop gain, infinite input resistance, zero output resistance)?

b. What is the input resistance of the amplifier?

c. What is the value of the voltage gain for a signal with 10 kΩ source resistance?



$$V_+ = 0 \Rightarrow V_- = 0$$

$$i_i = \frac{V_i - 0}{10k\Omega} = \frac{-(V_i - 0)}{10k\Omega}$$

$$\Rightarrow \frac{V_o}{V_i} = -\frac{1M\Omega}{10k\Omega} = -100 \text{ (V/V)}$$

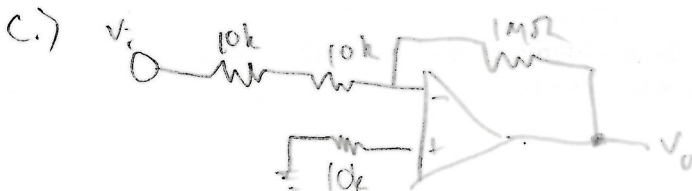
$$\boxed{\frac{V_o}{V_i} = -100 \text{ (V/V)}} \quad (8)$$

final numbers
account for 2
points each
sub question

b.)

$$i_i = \frac{V_i}{10k} \Rightarrow R_{in} \equiv \frac{V_i}{i_i} = 10k\Omega$$

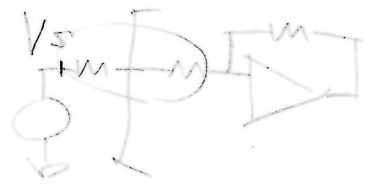
$$\boxed{R_{in} = 10k\Omega} \quad (6)$$



$$\frac{V_o}{V_i} = A_v \left(\frac{R_{in}}{R_{in} + R_{cs}} \right) = -100 \cdot 0.5 = -50$$

$$\Rightarrow \boxed{\frac{V_o}{V_i} = -50 \text{ (V/V)}} \quad (6)$$

2. For the same circuit as in Problem 1 and the same source resistance, but consider an Op Amp with a finite open loop gain of $A_0 = 100,000$, and an open-loop bandwidth of 100 Hz. The input resistance of the Op Amp is still infinite, and the output resistance is zero.
- What is the 3-dB frequency of the amplifier in unit of Hz?
(You don't need to re-derive the expression if you can deduce the frequency response of the close-loop amplifier).
 - Show the frequency response in Bode plot. Mark the 3-dB frequency, unity gain frequency, the low frequency gain in dB, and the slope in dB/decade.



a.) Fixed gain-bandwidth product

$$|A| \cdot f_{3dB} = 10^5 \cdot 10^2 \text{ Hz} = 10^7 \text{ Hz}$$

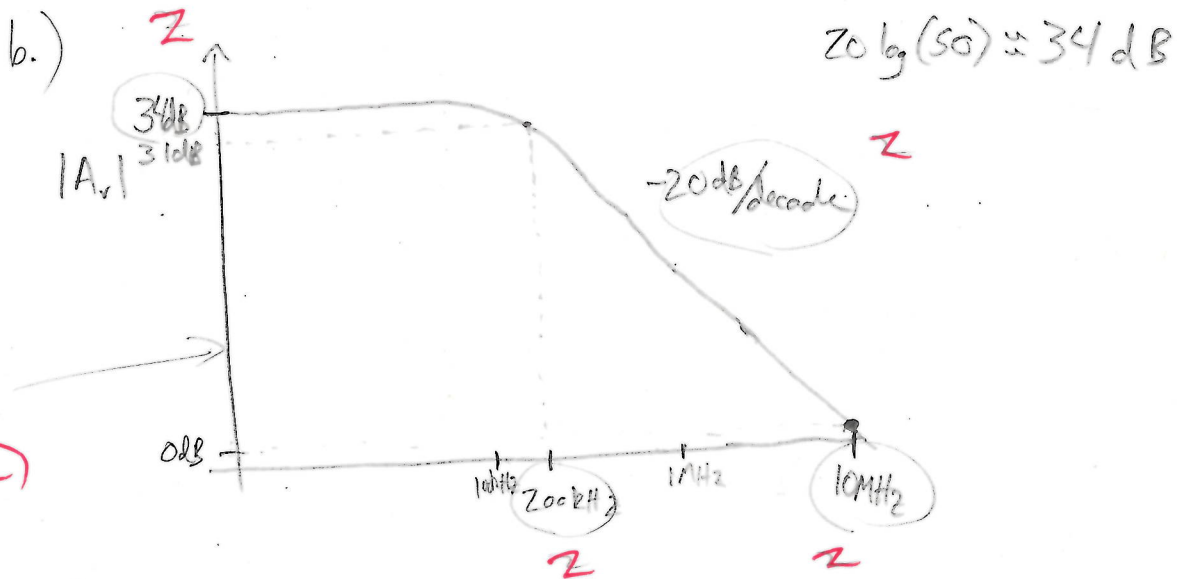
Amplifier in Prob. 1 $|A| = 50$

$$\Rightarrow f_{3dB} = \frac{10^7}{|A|} = \frac{10^7}{50} = 2 \cdot 10^5 = 200 \text{ kHz}$$

-5 if neglect source resistance

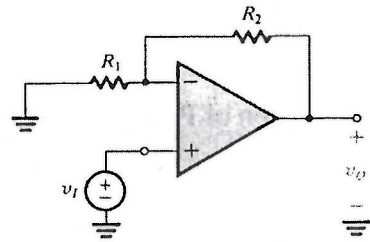
$$f_{3dB} = 200 \text{ kHz}$$

$$\frac{10^7}{100} = 10^5 \text{ Hz} = 100 \text{ kHz}$$



Half points deducted for carryover from part a)

3. A non-inverting amplifier with variable gain is shown on the right. Here, $R_1 = 1 \text{ k}\Omega$ and R_2 is variable from $100 \text{ k}\Omega$ to $100 \text{ M}\Omega$. This input signal is:



$$v_i(t) = (10 \text{ mV}) \cdot \sin(2\pi \cdot 10 \text{ kHz} \cdot t).$$

The Op Amp has a slew rate (SR) of $6.28 \text{ V}/\mu\text{s}$.

- First, assume the Op Amp has infinite bandwidth. If we gradually increase the gain of the amplifier by increasing R_2 , at what value of R_2 does the output become slew rate limited?
- Now consider the Op Amp with a finite gain-bandwidth product of 100 MHz and $R_2 = 20 \text{ M}\Omega$, is the amplifier bandwidth-limited or SR-limited? Show the calculation supporting your answer.

a. Gain $A_v = 1 + \frac{R_2}{R_1}$ *account for 2/4*

$$V_o = A_v \cdot v_i$$

$$\left. \frac{dV_o}{dt} \right|_{\text{max}} = A_v \cdot 10 \text{ mV} \cdot 2\pi \cdot 10 \text{ k} \cdot \cos(2\pi \cdot 10 \text{ k} t) \Big|_{2\pi \cdot 10 \text{ k} t = 0}$$

accounts for 2/4

$$= A_v \cdot 10 \text{ mV} \cdot 2\pi \cdot 10 \text{ k} \leq \text{SR} = 6.28 \text{ V}/\mu\text{s}$$

$$= 2\pi \cdot 10000 \cdot 10^{-2}$$

final number 2

$$A_v \leq \frac{10^2}{0.01} = 10^4 \Rightarrow R_2 \leq 10 \text{ M}\Omega \quad (10)$$

b. Given $R_2 = 20 \text{ M}\Omega$, $A_{v0} = 1 + \frac{20 \text{ M}}{1 \text{ k}} \approx 2 \times 10^4$ *account for 3 points*

$$f_{3\text{dB}} = \frac{100 \text{ MHz}}{2 \times 10^4} = 5 \text{ kHz} < 10 \text{ kHz}$$

At first, the Op Amp is BW limited (5)

then, consider the BW caused attenuation

if answer SR limited (with math) but forget BW attenuation penalty -2

$$A_v @ 10 \text{ kHz} = \frac{A_{v0}}{\sqrt{1 + \left(\frac{f}{f_{3\text{dB}}}\right)^2}} \Big|_{f=10 \text{ kHz}} = \frac{2 \times 10^4}{\sqrt{5}}$$

$$\text{So } \left. \frac{dV_o}{dt} \right|_{\text{max}} = \frac{2 \times 10^4}{\sqrt{5}} \times 10 \text{ mV} \cdot 2\pi \cdot 10 \text{ k} < \text{SR}$$

NO SR limited (5)

4. A pn junction in the reverse-bias configuration can be used as a variable capacitor. In the lab, we measured the capacitances of a pn junction diode at two voltages:
- (1) At 2.4 V reverse bias, the capacitance is measured to be 0.5 pF
 - (2) At 12 V reverse bias, the capacitance is measured to be 0.25 pF
- a. Find the capacitance of the pn junction diode at zero bias.
 - b. Find the built-in potential of the pn junction diode.

$$\text{Given: } C_{j0} = A \sqrt{\frac{\epsilon_s q}{2}} \frac{N_A N_D}{(N_A + N_D)} \cdot \frac{1}{\sqrt{V_0}}$$

$$= \frac{\alpha}{2\sqrt{V_0}}$$

We know with reverse bias $V_0 \Rightarrow V_0 + V_R$

$$\Rightarrow C_j = \frac{\alpha}{2\sqrt{V_0 + V_R}}$$

$$\Rightarrow C_j = \frac{C_{j0} \cdot \sqrt{V_0}}{\sqrt{V_0 + V_R}} = \frac{C_{j0}}{\sqrt{1 + \frac{V_R}{V_0}}}$$

$$C_j^2 \left(1 + \frac{V_R}{V_0}\right) = C_{j0}^2$$

@ $V_R = 2.4 \text{ V}$, $C_j = 0.5 \text{ pF}$

$$\Rightarrow .25 \left(1 + \frac{2.4}{V_0}\right) = C_{j0}^2$$

@ $V_R = 12 \text{ V}$, $C_j = 0.25 \text{ pF}$

$$\Rightarrow .0625 \left(1 + \frac{12}{V_0}\right) = C_{j0}^2 = .25 \left(1 + \frac{2.4}{V_0}\right)$$

$$1 + \frac{12}{V_0} = 4 + \frac{9.6}{V_0} \Rightarrow V_0 + 12 = 4V_0 + 9.6$$

$$\Rightarrow 3V_0 = 2.4, \quad \boxed{V_0 = 0.8 \text{ V}}$$

$$C_{j0}^2 = .25 \left(1 + \frac{2.4}{.8}\right) = 1 \Rightarrow \boxed{C_{j0} = 1 \text{ pF}}$$

-2 if close w/ correct approach
-5 if correct approach but not close

10

10

5. Consider the following two one-sided pn junction diodes with opposite doping profiles:

Diode A: $N_D = 10^{18} \text{ cm}^{-3}$, $N_A = 10^{16} \text{ cm}^{-3}$

Diode B: $N_D = 10^{16} \text{ cm}^{-3}$, $N_A = 10^{18} \text{ cm}^{-3}$

The rest of the material parameters are

shown in the table. Other parameters (e.g., junction area) of the two diodes are identical.

Electron diffusion coefficient	D_n	$30 \text{ cm}^2/\text{s}$
Hole diffusion coefficient	D_p	$10 \text{ cm}^2/\text{s}$
Electron diffusion length	L_n	$2 \text{ }\mu\text{m}$
Hole diffusion length	L_p	$1 \text{ }\mu\text{m}$

- a. What is the *ratio* of the current going through the diodes under a forward bias voltage of 0.8V?

- b. What is the *difference* of the built-in voltages between these two diodes?

- c. What is the *ratio* of the diode capacitances at zero bias?

8.)

Diode current eqn: $I = A q n_i^2 \left(\frac{D_p}{L_p N_D} + \frac{D_n}{L_n N_A} \right) (e^{V/V_T} - 1)$

Diode A: $I_A \approx I_n = A q n_i^2 \frac{D_n}{L_n N_A} (e^{V/V_T} - 1)$

Diode B: $I_B \approx I_p = A q n_i^2 \frac{D_p}{L_p N_D} (e^{V/V_T} - 1)$

$\Rightarrow \frac{I_A}{I_B} = \frac{D_n}{D_p} \cdot \frac{L_p}{L_n} \cdot \frac{N_D}{N_A} = \frac{30}{10} \cdot \frac{1}{2} \cdot \frac{10^{16}}{10^{18}} = \boxed{\frac{3}{2}}$

~~Factor~~ wrong number
take 2
points off

6.)

$V_0 = V_T \ln \left(\frac{N_A N_D}{n_i^2} \right)$

$N_A N_D = 10^{16} \cdot 10^{18} = 10^{34}$ for both diodes

$\Rightarrow V_{0A} = V_{0B} \Rightarrow V_{0A} - V_{0B} = \boxed{0V}$

6.)

$C_{j0} = A \sqrt{\frac{\epsilon_s \alpha}{2}} \frac{N_A N_D}{N_A + N_D} \frac{1}{\sqrt{V_0}}$

$\frac{N_A N_D}{N_A + N_D}$ is the same for both A and B

$V_{0A} = V_{0B}$

$\Rightarrow C_{j0A} = C_{j0B}$

$\Rightarrow \frac{C_{j0A}}{C_{j0B}} = \boxed{1}$