

Energy Balance (total)

$$\frac{dE}{dt} = \dot{Q} + \dot{W}_s - F_{A0,1} \left(\sum_i \theta_i C_{pi} \right) (T_1 - T_1) - F_{C0,2} \left(\sum_i \theta_i C_{pi} \right) (T_1 - T_{0,2}) - F_{A0,1} X_{A1} \Delta H_{R1}^\circ - F_{C0,2} X_{C2} \Delta H_{R2}^\circ$$

→ Steady, no shaft work, adiabatic (to surroundings), $T_1 = T_{0,2}$

$$0 = -F_{A0,1} X_{A1} \Delta H_{R1}^\circ - F_{C0,2} X_{C2} \Delta H_{R2}^\circ$$

Mole Balance on CSTR2

$$X_{C2} = \frac{k_2 \tau}{1 + k_2 \tau} = \frac{k_2 \left(\frac{V_2 C_{C0,2}}{F_{C0,2}} \right)}{1 + k_2 \left(\frac{V_2 C_{C0,2}}{F_{C0,2}} \right)}$$

Sub in

$$\frac{k_2 V_2 C_{C0,2}}{1 + k_2 \frac{V_2 C_{C0,2}}{F_{C0,2}}} (\Delta H_{R2}^\circ) = -F_{A0,1} X_{A1} \Delta H_{R1}^\circ$$

$$F_{C0,2} = \frac{-k_2 V_2 C_{C0,2}}{\frac{k_2 V_2 C_{C0,2} \Delta H_{R2}^\circ}{F_{A0,1} X_{A1} \Delta H_{R1}^\circ} + 1}$$

$$F_{CO_2} = \frac{(-0.5 \text{ min}^{-1})(100 \text{ L})(3 \text{ mol L}^{-1})}{(0.5 \text{ min}^{-1})(100 \text{ L})(3 \text{ mol L}^{-1})(25000 \text{ J mol}^{-1}) + 1}$$

$$\frac{(0.5 \text{ min}^{-1})(100 \text{ L})(3 \text{ mol L}^{-1})(25000 \text{ J mol}^{-1})}{(50 \text{ mol min}^{-1})(0.67)(-50000 \text{ J mol}^{-1})} + 1$$

$$F_{CO_2} = 121 \text{ mol min}^{-1}$$

Part b)

Energy Balance (steady, no shaft work, adiabatic to surroundings)

$$0 = -F_{CO_2} C_p (T_1 - T_{0,2}) - F_{AO_1} X_{A1} \Delta H_{R1}^{\circ} - F_{CO_2} X_{C2} \Delta H_{R2}^{\circ}$$

$$0 = -F_{CO_2} C_p (T_1 - T_{0,2}) - F_{AO_1} X_{A1} \Delta H_{R1}^{\circ} - F_{CO_2} \left(\frac{k_2 \frac{V_2 C_{CO}}{F_{CO}}}{1 + k_2 \frac{V_2 C_{CO}}{F_{CO}}} \right) \Delta H_{R2}^{\circ}$$

$$F_{AO_1} X_{A1} \Delta H_{R1}^{\circ} = -F_{CO_2} C_p (T_1 - T_{0,2}) - F_{CO_2} \left(\frac{k_2 \frac{V_2 C_{CO}}{F_{CO}}}{1 + k_2 \frac{V_2 C_{CO}}{F_{CO}}} \right) \Delta H_{R2}^{\circ}$$

The rate of heat generated by system (1) must be consumed by system (2).

Decreasing the inlet T of system (2) requires that some of the heat generated in (1)

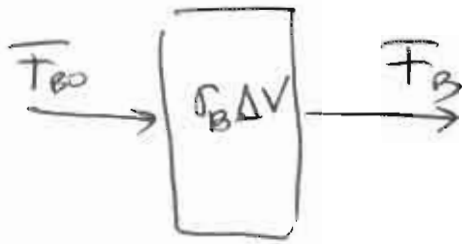
be used to heat the feed to the reactor temperature (T_1). As a result, less

heat is consumed by the endothermic reaction in (2), designated by the $F_{CO_2} X_{C2}$ term &

$$F_{CO_2} X_{C2} = \frac{k_2 V_2 C_{CO}}{1 + k_2 V_2 C_{CO}} \rightarrow F_{CO} \text{ must decrease}$$

Problem 2

(a)



$$r = k C_B^2$$

$$r_B = -2k C_B^2$$

$$F_{B0} + r_B \Delta V - F_B = 0$$

$$F_{B0} X_B = -r_B \Delta V$$

$$C_{B0} X_B = -r_B \tau_0$$

$$\tau_0 = \frac{C_{B0} X_B}{-r_B} = \frac{C_{B0} X_B}{2k C_B^2}$$

$$C_B = C_{B0} \frac{(\cancel{V} X)}{(1 + \cancel{E} X)} \cdot \left(\frac{T_0}{T} \right) \left(\frac{\cancel{P}}{P_0} \right)^1 = C_{B0} \left(\frac{T_0}{T} \right)$$

~ 1
for low X

$$\tau_0 = \frac{\cancel{C}_{B0} X_B}{2k(T) \cancel{C}_{B0}^2} \left(\frac{T}{T_0} \right)^2 = \frac{X_B \nu_0}{2A \exp\left(-\frac{E_a}{RT}\right) C_{B0}} \left(\frac{T}{T_0} \right)^2$$

(b) If $X = 0.9$ our expression won't apply because we won't be able to assume an uniform concentration and temperature throughout the reactor.

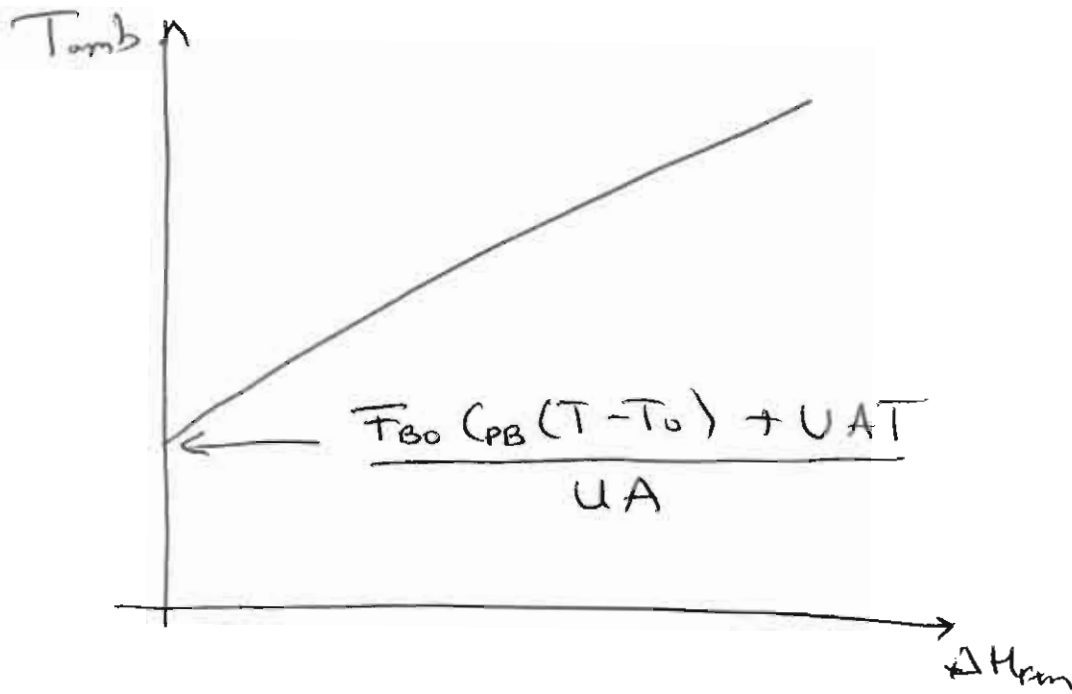
(c)

Energy Balance

$$UA(T - T_{amb}) + \bar{F}_{B0} X_B \Delta H_{rxn} + \bar{F}_{B0} C_{PB}(T - T_0) = 0$$

$$\Delta C_p = 0 = C_{p,c} - 2C_{p,B} \Rightarrow \Delta H_{rxn} = \Delta H_{rxn}^0$$

$$\Rightarrow T_{amb} = \frac{\bar{F}_{B0} X_B \Delta H_{rxn}^0 + \bar{F}_{B0} C_{PB}(T - T_0) + UA T}{UA}$$



Problem 3

$$r = \frac{r_c}{1/2} = 2r_c = 2k_c \frac{C_{cs}^2}{C_T}$$

$$K_B = \frac{C_{cs}}{C_{AS} \cdot P_B}$$

$$C_{AS} = K_A P_A C_S$$

$$C_{cs} = K_B P_B C_{AS} = K_B K_A P_B P_A C_S$$

site balance:

$$C_T = C_S + C_{AS} + C_{cs} + C_{DS}$$

$$C_{DS} = \frac{P_D \cdot C_S}{K_D}$$

$$C_T = \left(1 + K_A P_A + K_B K_A P_B P_A + \frac{P_D}{K_D} \right) C_S$$

$$C_S = \frac{C_T}{\square}$$

$$C_{cs} = K_B K_A P_B P_A \frac{C_T}{\square}$$

$$r = \frac{2k_c (K_B K_A P_B P_A)^2 C_T}{\left(1 + K_A P_A + K_B K_A P_B P_A + P_D/K_D \right)^2}$$

(b) If S is MASI

$$C_T \approx C_S$$

$$C_{CS} = K_B K_A P_B P_A C_T$$

$$r = 2 k_c (K_B K_A P_B P_A)^2 C_T$$

(c) $k_{\text{eff}} = 2 k_c K_B K_A C_T$

$$\frac{d \ln k_{\text{eff}}}{d(1/T)} = - \frac{E_c + \Delta H_B + \Delta H_A}{R}$$

$$E_{\text{app}} = E_c + \Delta H_B + \Delta H_A$$