

Problem 1

a.) The relevant equation for conductive heat transfer is:

$$\frac{\Delta Q}{\Delta t} = kA \frac{\Delta T}{\Delta x}$$

At the junction, given that there are no fluctuations in time, we have:

$$\left(\frac{\Delta Q}{\Delta t} \right)_{\text{slab 1}} = \left(\frac{\Delta Q}{\Delta t} \right)_{\text{slab 2}}$$

so that:

$$k_1 A \frac{T_H - T_J}{L_1} = k_2 A \frac{T_J - T_C}{L_2}$$

Solving for T_J , we have:

$$T_J = \frac{T_H k_1 / L_1 + T_C k_2 / L_2}{k_1 / L_1 + k_2 / L_2}$$

b.) The rate of heat transfer into the ice is:

$$\frac{\Delta Q}{\Delta t} = k_2 A \frac{T_J - T_C}{L_2}$$

The amount of heat required to melt the ice is:

$$\Delta Q = ML_F$$

Therefore the time required to melt it is:

$$\Delta t = \frac{\Delta Q L_2}{k_2 A (T_J - T_C)} = \frac{ML_F L_2}{k_2 A \left(\frac{T_H k_1 / L_1 + T_C k_2 / L_2}{k_1 / L_1 + k_2 / L_2} - T_C \right)}$$

Problem 2

We remember Archimedes' principle (i.e. buoyancy = weight of displaced fluid). This gives us the relations between the initial densities:

$$\rho_{\text{sphere}} \cdot V_{\text{sphere}} = \rho_{\text{liquid}} \cdot \frac{1}{2} V_{\text{sphere}} \Rightarrow \rho_{\text{sphere}} = \frac{1}{2} \rho_{\text{liquid}}$$

At neutral buoyancy we have:

$$\rho'_{\text{sphere}} = \rho'_{\text{liquid}}$$

Therefore we have:

$$\frac{m_{\text{sphere}}}{V_{\text{sphere}} + \Delta V_{\text{sphere}}} = \frac{m_{\text{liquid}}}{V_{\text{liquid}} + \Delta V_{\text{liquid}}}$$

Plugging in the initial density values:

$$2(1 + \Delta V_{\text{sphere}}/V_{\text{sphere}}) = 1 + \Delta V_{\text{liquid}}/V_{\text{liquid}}$$

Using the fact that $\Delta V/V = \beta \Delta T$:

$$\beta_L = 2\beta_S + \frac{1}{\Delta T}$$

Problem 3

The heat lost by the skewer has to equal the heat gained by the water, so:

$$M_S c_S (T_H - T_F) = M_W c_W (T_F - T_W) \quad (1)$$

which gives

$$T_F = \frac{M_S c_S T_H + M_W c_W T_W}{M_S c_S + M_W c_W}. \quad (2)$$

Using $dQ = M_S c_S dT$, the entropy change of the skewer is

$$\Delta S_S = \int \frac{dQ}{T} = \int \frac{M_S c_S dT}{T} = M_S c_S \ln \frac{T_F}{T_S} < 0. \quad (3)$$

In exactly the same way we get for the water:

$$\Delta S_W = M_W c_W \ln \frac{T_F}{T_W} > 0. \quad (4)$$

The total entropy change is then

$$\Delta S_{TOT} = M_S c_S \ln \frac{T_F}{T_S} + M_W c_W \ln \frac{T_F}{T_W} \quad (5)$$

which we know to be positive by the Second Law of Thermodynamics.

Problem 4

- For AB , $Q = 0$ because the process is adiabatic. Work $W_{AB} = \int p dV$ is positive.
- Using $Q = \Delta E_{int} + W$, for BC , $\Delta E_{int} = \frac{d}{2} N k_B \Delta T = 0$ because it is isothermal, and $W < 0$ because the gas is being compressed, so $Q < 0$ and heat is leaving the system.
- For CA , $W = 0$ (the volume is constant), and temperature is increasing, so $Q > 0$ and heat is entering the system.

Point A has the highest temperature, and point B has the lowest. This can be seen by plotting isotherms, and remembering that for an adiabat $p \propto \frac{1}{V^\gamma}$ which falls more quickly than an isotherm, so $T_A > T_B$.

Carnot efficiency is:

$$e_C = 1 - \frac{T_L}{T_H}. \quad (6)$$

T_H is just $T_A = \frac{P_A V_A}{nR}$. Note that $T_L = T_B = T_C$, so since AB is adiabatic we have:

$$P_A V_A^\gamma = P_B (2V_A)^\gamma \implies P_B = \frac{P_A}{2^\gamma} \quad (7)$$

Hence $T_B = \frac{P_B V_B}{nR} = \frac{P_A V_A}{2^{\gamma-1} nR}$ which gives:

$$e_C = 1 - \frac{1}{2^{\gamma-1}} = 1 - 2^{1-\gamma} \quad (8)$$

The only heat flow in is along CA and is given by $Q_{IN} = nC_V \Delta T = \frac{d}{2} nR(T_A - T_C) = \frac{1}{\gamma-1} nRT_A (1 - 2^{1-\gamma}) = \frac{1}{\gamma-1} P_A V_A (1 - 2^{1-\gamma})$ where we have used the relation between d and γ on the formula sheet. The work done during AB is:

$$W_{AB} = -\Delta E_{int} = -\frac{d}{2} nR(T_B - T_A) = \frac{1}{\gamma-1} P_A V_A (1 - 2^{1-\gamma}). \quad (9)$$

The work done during the isothermal compression BC is:

$$W_{BC} = nRT_C \ln \left(\frac{V_B}{V_A} \right) = -2^{1-\gamma} P_A V_A \ln 2. \quad (10)$$

Finally then the efficiency is:

$$e = \frac{W_{NET}}{Q_{IN}} = \frac{P_A V_A \left(\frac{1}{\gamma-1} (1 - 2^{1-\gamma}) - 2^{1-\gamma} \ln 2 \right)}{P_A V_A \frac{1}{\gamma-1} (1 - 2^{1-\gamma})} \quad (11)$$

which can be written

$$e = 1 - \frac{2^{1-\gamma} (\gamma - 1) \ln 2}{(1 - 2^{1-\gamma})} \quad (12)$$

a)

The electric field on the axis is

$$\vec{E}(x) = \frac{1}{4\pi\epsilon_0} \left(\frac{Q_1}{x^2} - \frac{Q_2}{(x-a)^2} \right) \hat{x}$$

Setting this equal to zero gives

$$(Q_1 - Q_2)x^2 - 2Q_1ax + Q_1a^2 = 0$$

The solution to this is

$$P_{\pm} = \frac{2aQ_1 \pm \sqrt{4a^2Q_1^2 - 4(Q_1 - Q_2)Q_1a^2}}{2(Q_1 - Q_2)} = a \frac{Q_1 \pm \sqrt{Q_1Q_2}}{Q_1 - Q_2}$$

We take the solution with the + sign as we want an answer > 0 .

$$P = a \frac{\sqrt{Q_1}}{\sqrt{Q_1} - \sqrt{Q_2}}$$

b)

The electric field of a point charge has no zeros so the force of a point charge on another cannot be zero. The force of Q_3 on Q_2 will be

$$\vec{F}_{32} = \frac{Q_2Q_3}{4\pi\epsilon_0a^2} \left(1 - \frac{\sqrt{Q_1}}{\sqrt{Q_1} - \sqrt{Q_2}} \right)^{-2} \hat{x} = \frac{Q_2Q_3}{4\pi\epsilon_0a^2} \left(1 - \sqrt{\frac{Q_1}{Q_2}} \right)^2 \hat{x}$$

c)

The force of Q_3 on Q_1 will be

$$\vec{F}_{31} = \frac{Q_1Q_3}{4\pi\epsilon_0a^2} \left(\frac{\sqrt{Q_1}}{\sqrt{Q_1} - \sqrt{Q_2}} \right)^{-2} (-\hat{x}) = -\frac{Q_1Q_3}{4\pi\epsilon_0a^2} \left(1 - \sqrt{\frac{Q_2}{Q_1}} \right)^2 \hat{x}$$

d)

We need \vec{F}_{21} to be equal in magnitude to the answer in part c (or equivalently \vec{F}_{12} to be equal in magnitude to the answer in part b). This is satisfied when

$$\frac{Q_1}{4\pi\epsilon_0} \frac{Q_2}{a^2} = \frac{Q_1}{4\pi\epsilon_0} \frac{Q_3}{P^2}$$

This means

$$Q_2 = \frac{Q_3}{Q_1} (\sqrt{Q_1} - \sqrt{Q_2})^2$$

So we need

$$Q_3 = \frac{Q_2Q_1}{(\sqrt{Q_1} - \sqrt{Q_2})^2}$$