

(i) AMPERE'S LAW:

17 pts.

$$\frac{d}{dt}(\epsilon_0 \vec{E}) = \vec{\nabla} \times \frac{\vec{B}}{\mu_0}$$

ARBITRARY ORIENTATION
IN Y-Z PLANE NOT GIVEN

$$\vec{\nabla} \times \vec{B} = -\mu_0 \epsilon_0 \omega E_0 \cos(kx - \omega t) \hat{y} \quad \left. \begin{array}{l} \downarrow \\ \end{array} \right\} \epsilon = \frac{1}{\sqrt{\mu_0 \epsilon_0}}$$

$$= -\frac{\omega}{c} \frac{E_0}{c} \frac{1}{k} \frac{d}{dx} \sin(kx - \omega t) \hat{y}$$

$$\hat{x} \times \hat{z} = -\hat{y}$$

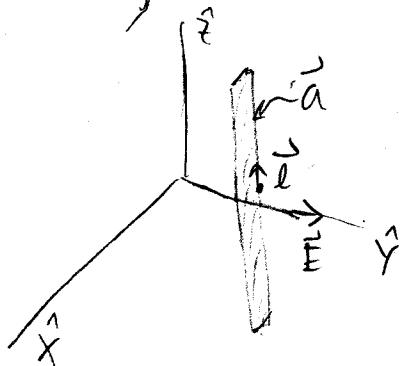
$$\Rightarrow \vec{B} = \frac{E_0}{c} \sin(kx - \omega t) \hat{z}$$

$\left. \begin{array}{l} \uparrow \\ \downarrow \end{array} \right\}$
 DIRECTION NOT
 REQUIRED

INTEGRAL METHOD:

$$\frac{d}{dt} \int (\epsilon_0 \vec{E}) \cdot d\vec{a} = \oint \frac{\vec{B}}{\mu_0} \cdot d\vec{\ell}$$

$$\Rightarrow \oint \vec{B} \cdot d\vec{\ell} = \int (\epsilon_0 \mu_0 \frac{d}{dt} \vec{E}) \cdot d\vec{a}$$



SO \vec{B} IS $\propto \hat{x}$ OR \hat{z}

NEXT
→

BUT

$$\oint \vec{E} \cdot d\vec{l}' = - \frac{d}{dt} \int \vec{B} \cdot d\vec{a}'$$

$$\text{So } \vec{B} \propto \hat{y} \text{ OR } \hat{z} \Rightarrow \vec{B} \propto \hat{z}$$

$$\Rightarrow \text{(BOUNDARY DERIVATIVE)} \quad \vec{B} = \epsilon_0 \mu_0 \frac{d}{dt} \vec{E}$$

$$\Rightarrow \text{GIVING SAME RESULT} \quad \vec{B} = - \int dx \epsilon_0 \mu_0 \frac{d}{dt} \vec{E}$$

(ii) 8 pts.

$$\nabla^2 \vec{E} = + \frac{1}{c^2} \frac{\partial^2}{\partial t^2} \vec{E}$$

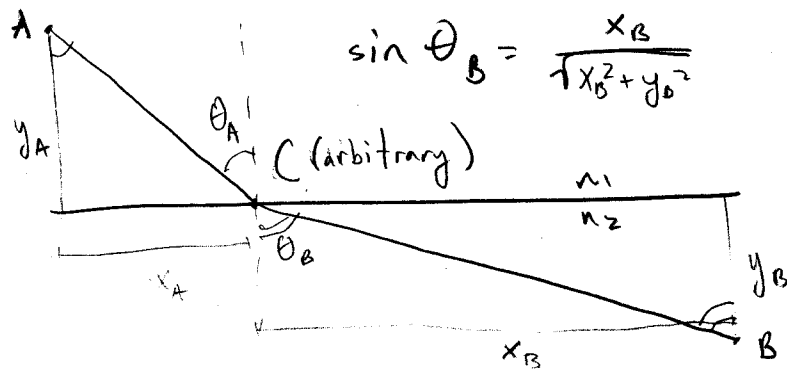
$$-k^2 E_0 \sin(kx - \omega t) = + \frac{1}{c^2} (-\omega^2) E_0 \sin(kx - \omega t)$$

$$c^2 = \frac{\omega^2}{k^2} \quad \checkmark$$

$$2.) v = \frac{c}{n}$$

$$\sin \theta_A = \frac{x_A}{\sqrt{x_A^2 + y_A^2}}$$

$$\sin \theta_B = \frac{x_B}{\sqrt{x_B^2 + y_B^2}}$$



$$t = \frac{d_A}{v_A} + \frac{d_B}{v_B} = \frac{n_1}{c} \sqrt{x_A^2 + y_A^2} + \frac{n_2}{c} \sqrt{x_B^2 + y_B^2}$$

For fixed A, B, the quantities $x \equiv x_A + x_B$, y_A , and y_B are fixed.

$$\Rightarrow t = \frac{n_1}{c} \sqrt{x_A^2 + y_A^2} + \frac{n_2}{c} \sqrt{(x - x_A)^2 + y_B^2}$$

Minimum time occurs when $\frac{dt}{dx_A} = 0$.

$$\Rightarrow 0 = \frac{n_1 x_A}{\sqrt{x_A^2 + y_A^2}} - \frac{n_2 (x - x_A)}{\sqrt{(x - x_A)^2 + y_B^2}}$$

$$= \frac{n_1 x_A}{\sqrt{x_A^2 + y_A^2}} - \frac{n_2 x_B}{\sqrt{x_B^2 + y_B^2}}$$

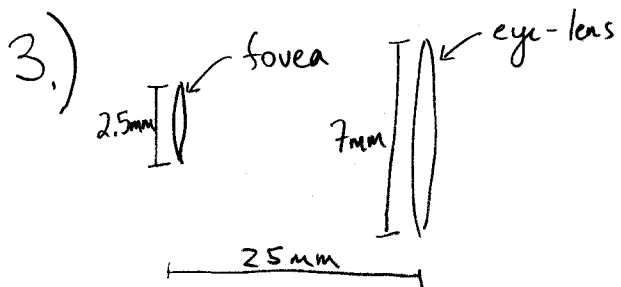
$$= n_1 \sin \theta_A - n_2 \sin \theta_B$$

$$\Rightarrow \boxed{n_1 \sin \theta_A = n_2 \sin \theta_B}$$

For reflection, calculations are the same, but the 2nd line is also in medium 1, so $n_1 \sin \theta_A = n_1 \sin \theta_B$

$$\Rightarrow \sin \theta_A = \sin \theta_B$$

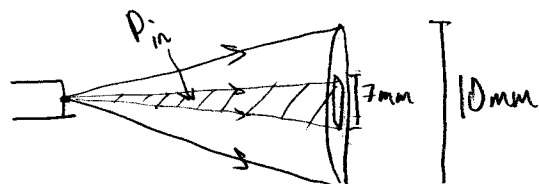
$$\Rightarrow \boxed{\theta_A = \theta_B}$$



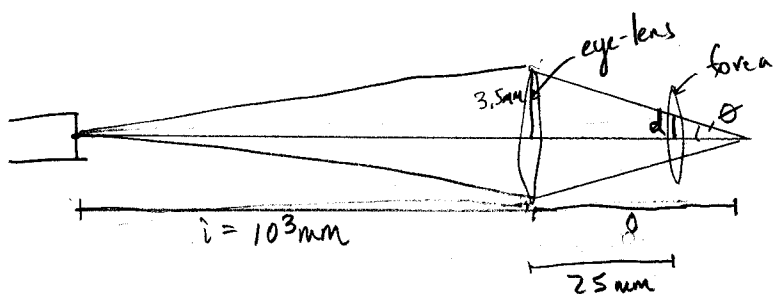
i.) lens-makers formula: $\frac{1}{f} = \left(\frac{n_{\text{lens}}}{n_{\text{outside}}} - 1 \right) \left(\frac{1}{r_2} - \frac{1}{r_1} \right)$

For $\frac{1}{r_1} = -\frac{1}{r_2}$, $\frac{1}{f} \approx \left(\frac{1.5}{1} - 1 \right) \left(\frac{2}{r_2} \right) = \frac{1}{r_2} \Rightarrow \boxed{r_2 \approx f = 25 \text{ mm}}$

iii.) $\tau \approx .25 \text{ s}$



$$P_{\text{in}} = 3 \text{ mW} \left(\frac{\pi (7 \text{ mm})^2 / 4}{\pi (10 \text{ mm})^2 / 4} \right) \approx \underline{1.47 \text{ mW}}$$



(not drawn to scale!)

$$\frac{1}{i} + \frac{1}{o} = \frac{1}{f} \Rightarrow o = \frac{if}{i-f} \approx 25.64 \text{ mm}$$

$$\tan \theta = \frac{3.5 \text{ mm}}{o} = \frac{d}{o - 25 \text{ mm}} \Rightarrow d = \left(1 - \frac{25 \text{ mm}}{o} \right) 3.5 \text{ mm} = .0875 \text{ mm}$$

$\Rightarrow d < 1.25 \text{ mm}$ (radius of fovea), so

all of "P_{in}" focuses to spot of radius d

$$\Rightarrow \text{irradiance} = \frac{P_{\text{in}}}{\pi d^2} \approx 61.1 \text{ mW/mm} = \boxed{6.1 \times 10^4 \text{ W/m}^2}$$

iii.) If the entire fovea weighs .1g, the spot weighs $(.1 \text{ g}) \left(\frac{\pi d^2}{\pi r^2} \right) \approx (.1 \text{ g}) \left(\frac{.0875}{1.25} \right)^2 \approx 4.9 \times 10^{-4} \text{ g}$

$$\Rightarrow \Delta T = \frac{\Delta E}{mC} = \frac{P_{\text{in}} \Delta t}{mC} = \frac{(1.47 \text{ mW})(.25 \text{ s})}{(4.9 \times 10^{-4} \text{ g})(45 \text{ J/g/C})} \approx \boxed{.2^\circ \text{ C}}$$

Or, if spot weighs .1g, $\Delta T = \frac{(1.47 \text{ mW})(.25 \text{ s})}{(.1 \text{ g})(45 \text{ J/g/C})} = \boxed{9.18 \times 10^{-4}^\circ \text{ C}}$

Grading Rubric:

#2 | 25 pts. total

- 7 pts. for finding time
- 18 pts. for deriving refl. $\&$ refraction laws using Fermat's principle
(8 pts. for reflection; 10 for refraction)

#3 | 25 pts. total

i.) 5 pts.

ii.) 5 pts. for getting "P_{in}"

5 pts. for finding spot size
and calculating irradiance

iii.) 5 pts.

} graded independently
(missing one piece doesn't directly
affect the others)

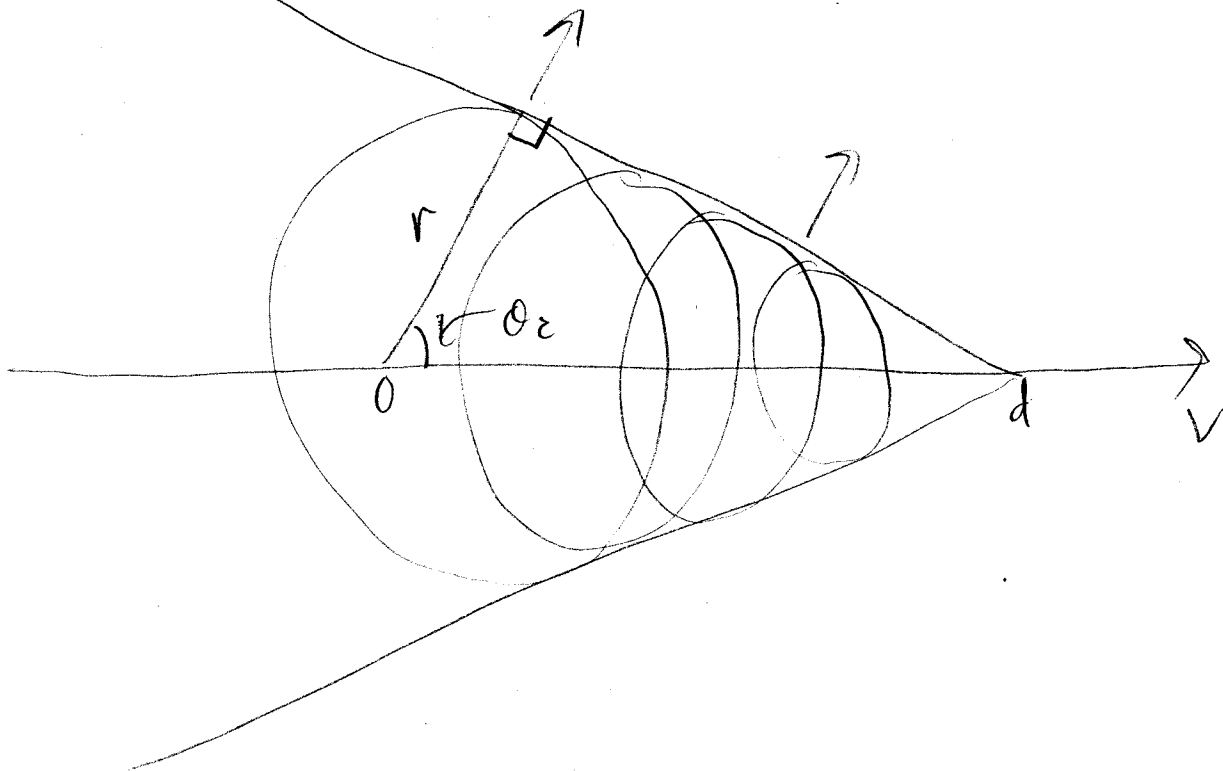
+ 5 pts. for correctly putting parts together and
getting correct final result

(note: students could assume either spot size or entire fovea weighs 1g
for part iii.; see solutions)

4

(i)

8 pts.



$$\cos \theta_c = \frac{r}{d} = \frac{\frac{d}{v} \cdot \frac{c}{n}}{d} = \frac{c}{vn} \checkmark$$

(ii)

4 pts.

$$\frac{c}{vn} < 1 \Rightarrow \left[\frac{v}{c} > \frac{1}{n} \right]$$

(iii)

13 pts.

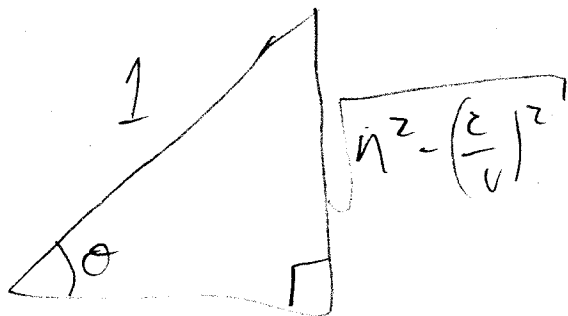
THERE IS REFRACTION:

$$n \sin \theta_c = \sin \theta; \quad \frac{R}{X_R} = \tan \theta \quad \text{dist. to screen}$$

$$\sin \theta_c = \sqrt{1 - \cos^2 \theta_c} = \sqrt{1 - \left(\frac{c}{vn}\right)^2}$$

$$\sin \theta = \sqrt{n^2 - \left(\frac{c}{v}\right)^2}$$

NEXT
→



$$\rightarrow \sqrt{1 - n^2 + \left(\frac{c}{v}\right)^2}$$

$$R = x \tan \theta = x \cdot \frac{n^2 - \left(\frac{c}{v}\right)^2}{\sqrt{1 - n^2 + \left(\frac{c}{v}\right)^2}}$$

$$= x \sqrt{\frac{\left(\frac{v}{c} n\right)^2 - 1}{1 - \left(\frac{v}{c}\right)^2 (n^2 - 1)}}$$

$$= 1 \text{ m} \sqrt{\frac{\left(\frac{2.5 \cdot 1.5}{3}\right)^2 - 1}{1 - \left(\frac{2.5}{3}\right)^2 (1.5^2 - 1)}}$$

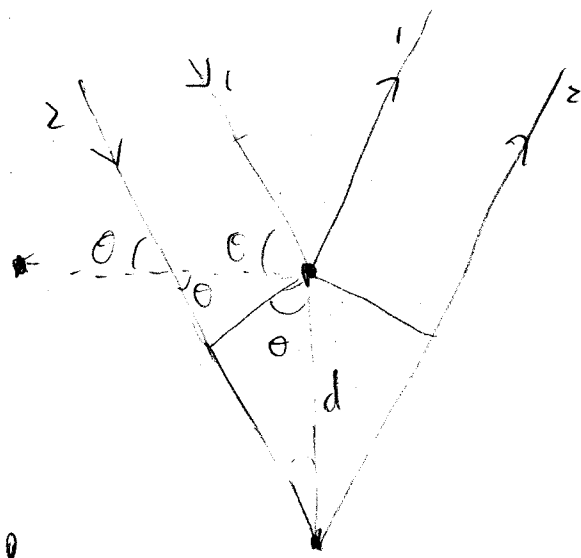
$$R \approx 2.06 \text{ m}$$

+ RADIOS AT EDGE OF GLASS = $0.75 \text{ cm} \cdot \tan \theta$
 $= 0.75 \text{ cm} \sqrt{\left(\frac{v n}{c}\right)^2 - 1}$

$$\Rightarrow \lceil 2.07 \text{ m} \rceil$$

5

(i)
15 pts.



$$\Delta X_{12} = 2(d \sin \theta) \Rightarrow n\lambda = 2d \sin \theta$$

THIS IS FOR ONE LAYER, BUT STACKING LAYERS YOU GET THE SAME RELATION

(ii)
7 pts.

$$\theta = \sin^{-1} \left(\frac{n\lambda}{2d} \right)$$

$$n=0: 0^\circ$$

$$n=1: 45.7^\circ$$

$$n=2: \text{---}$$

$$45.7^\circ \approx 0.8 \text{ (rad)}$$

(iii)
3 pts.

$$\frac{\lambda}{2d} < 1 \Rightarrow \lambda < 2d$$

$$\lambda < 0.215 \text{ nm} \quad \text{NO}_2$$