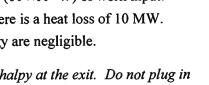
## QUIZ 3 SOLUTION - Phiteman

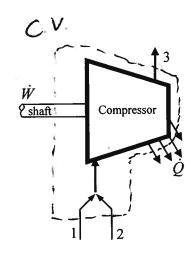
Problem 1 (20 pts)

A compressor has two inlets and one outlet:

Input 1 takes in saturated liquid water at  $T_1=70$  °C and  $\dot{m}_1=5$  kg/s Input 2 takes in saturated water vapor at  $T_2=70$  °C and  $\dot{m}_2=20$  kg/s. The outlet is at  $p_3 = 800 \text{ kPa}$ .

The compressor requires  $\dot{W} = 60 \text{ MW} (60 \times 10^6 \text{ W}) \text{ of work input.}$ The compressor is uninsulated, and there is a heat loss of 10 MW. Changes in kinetic and potential energy are negligible.





(a) Obtain a symbolic equation for the enthalpy at the exit. Do not plug in any numbers.

(b) What is the numerical value of temperature of the exiting stream,  $T_3$ ?

MASS: 
$$\frac{d}{dt}M_{cv} = \dot{m}_1 + \dot{m}_2 - \dot{m}_3 \Rightarrow \dot{m}_3 = \dot{m}_1 + \dot{m}_2$$

(a) Need 
$$h_1$$
:  $h_5(70^{\circ}C) = 293.1 \text{ kJ/kg} \rightarrow m_1 h_1 = 1,465.5 \text{ kW}$ 

$$h_2 : h_3(70^{\circ}C) = 2626.1 : \rightarrow m_2 h_2 = 52,522 \text{ kW}$$

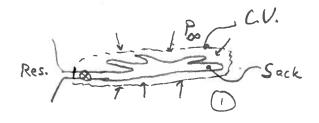
$$\Rightarrow h_3 = 4159.5 \text{ kJ}$$

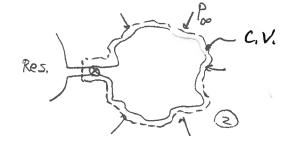
$$and p_3 = 800 \text{ kPa} = 0.8 \text{ MPa}.$$

$$S.H.V. Table \rightarrow T_3 \approx 800^{\circ}C \text{ (h=4157 kJ)}$$

## Problem 2 (20 pts)

A thin, flexible sack is connected by a valve to a reservoir of saturated water vapor at 120 °C. Initially the sack is completely empty. The valve is opened slightly and steam begins to fill the sack. After some time the sack volume has expanded to 0.50 m<sup>3</sup>. Weighing the sack reveals that its mass has increased by 0.23 kg. The pressure outside the sack is p<sub>∞</sub>=100 kPa throughout this process. There was also a heat transfer Q<sub>12</sub> (value unknown) between sack and surroundings during this process.





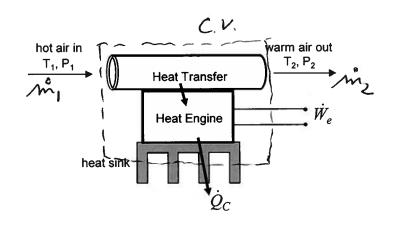
(b) What was the heat transfer  $Q_{12}$  in kJ? Clearly specify the magnitude and direction. empty

$$U = \frac{\sqrt{2}}{m_2} = \frac{0.5 \, \text{m}^3}{0.23 \, \text{kg}} = 2.17 \, \frac{\text{m}^3}{\text{kg}}.$$

## Problem 3 (20 pts)

(Background: devices like this are being considered to generate electricity from hot car exhaust.)

Hot air enters a pipe at  $T_1$ ,  $P_1$ , and exits at  $T_2$ ,  $P_2$ . A heat engine is mounted to the side of the pipe, such that there is a steady heat transfer from the pipe to the heat engine. The heat engine generates electrical power  $\dot{W}_e$ . The heat engine also rejects heat to the surroundings at a rate  $\dot{Q}_C$ 



## Given:

 $T_1, P_1, T_2, P_2,$ 

 $\dot{W}_e$ ,  $\dot{Q}_C$ ,

Air as an ideal gas, with constant C<sub>p</sub>, C<sub>v</sub>, and R

Derive an expression for the mass flow rate of air, in. You may ignore kinetic energy effects.

MASS:

d Mar = m, -m,

=> m,= m2

5.5

ENERGY:

de for = - Oc - we + m, h, - m2 h2 5.5.

m (h, -hz) = We + Qe

$$\mathring{m} = \frac{\mathring{w}_e + \mathring{Q}_c}{C_p(T_1 - T_2)}$$

Ideal gas, const. G: Sh = G ST (...more space for Problem 3)

E. C. ) Now add KE terms to m

0 = - Oc- @we + m(Ch, + \(\frac{1}{2}\) - (h\_2 + \(\frac{1}{2}\))

me We + Qc

(T1-12) +1 (V2-V22)

\* Which is faster, V, or Vz?

Mass: m= Av

(Extra Credit: 5 pts) If we did account for changes in kinetic energy, qualitatively how would the work output change? Other than  $\dot{W}_e$  and KE, assume all quantities given above remain constant. You must justify your answer.

- (i) Accounting for KE effects would cause  $W_e$  to increase.
- (ii) Accounting for KE effects would cause  $\dot{W}_e$  to stay the same.
- (iii) Accounting for KE effects would cause  $\dot{W}_e$  to decrease

$$W_{e} = -\hat{Q}_{c} + \hat{m} \left( p \left( T_{1} - \overline{I}_{2} \right) + \hat{m} \left( \frac{\hat{m}}{A_{c}} \frac{RT_{i}}{P_{i}} \right)^{2} - \left( \frac{\hat{m}}{A_{c}} R \frac{T_{2}}{P_{2}} \right)^{2} \right)$$

If  $\frac{T_1}{P_1} > \frac{T_2}{P_2}$ ; we incr. Weed more info to decode!

The true of the decode!

Realistically, Ap typically a few %, whereas Tang 7 10%

SO ST effect most likely to dominate. Expect Wo increase (most likely)