

MEAN 144/200
SD 36/200

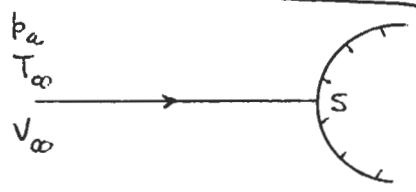
Full credit for correct final answer with coherent argument - otherwise partial credit as shown
SOLUTIONS

ME106 Fluid mechanics
2nd Test, S04

NAME _____

MEAN 52
SD 14

1. (65) Air at temperature $T_\infty = 293$ K and pressure $p_a = 101$ kPa flows at speed $V_\infty = 500$ m/s towards the stagnation point S. The specific heat ratio $\gamma = 1.4$, and the gas constant $R = 287$ J/kg·K. Find:



(a) the stagnation temperature T_0 ;

(20) $\frac{V^2}{2c_p} + T = T_0$ defines stagnation temp. T_0 ; evaluate LHS at ∞

$c_p = \frac{\gamma}{\gamma-1} R = 1004.5 \Rightarrow T_0 = \frac{(500)^2}{2009} + 293 = 417$ K $\Rightarrow T_0 = 417$ K

Stagnation temp.

(b) the stagnation pressure p_0 ^{at infinity} and

(20) $\frac{p}{p_0} = \left(\frac{T}{T_0}\right)^{\frac{\gamma}{\gamma-1}}$ for given p, T this defines stagnation pressure p_0 pressure in the stagnation chamber used to generate the flow p_∞, T_∞ . Solve for $p_0 = p_\infty \left(\frac{T_0}{T_\infty}\right)^{\frac{\gamma}{\gamma-1}} = 101 \times \left(\frac{417}{293}\right)^{\frac{1.4}{0.4}}$, $p_0 = 347$ kPa

stagnation pressure

(25) (c) the pressure p_s at the stagnation point.

From BE $V^2 = 2c_p T_0 \left(1 - \left(\frac{p}{p_0}\right)^{\frac{\gamma-1}{\gamma}}\right)$, $p_0 = p / \left(1 - \frac{V^2}{2c_p T_0}\right)^{\frac{\gamma}{\gamma-1}}$

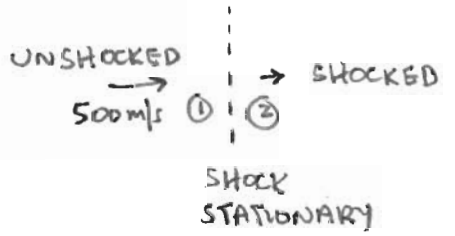
-10 Correct eq wrongly used

-5 Minor slip / so with correct approach

-5 Correct eq wrongly copied.

gives the stagnation pressure at a point with pressure p and speed V .

$$\frac{p_{02}}{p_{01}} = \frac{p_2}{p_1} \left(\frac{1 - \frac{V_1^2}{2c_p T_0}}{1 - \frac{V_2^2}{2c_p T_0}} \right)^{\frac{\gamma}{\gamma-1}}$$



(T_0 is same on both sides.)

Heat $T_1 = 293$ K $\Rightarrow c_1 = \sqrt{\gamma R T} = 343$, $V_1 = 500$ m/s $\Rightarrow M_1 = 1.46$

$\frac{V_1}{V_2} = \frac{(\gamma+1) M_1^2}{(\gamma-1) M_1^2 + 2} = 1.79 \Rightarrow V_2 = 280$ m/s

$\frac{p_2}{p_1} = 1 + \frac{2\gamma}{\gamma+1} (M_1^2 - 1) = 2.32 \Rightarrow \frac{p_{02}}{p_{01}} = 2.32 \times \left(\frac{1 - \frac{500^2}{2009 \times 417}}{1 - \frac{280^2}{2009 \times 417}} \right)^{3.5}$

PLEASE PRINT YOUR NAME ON THIS PAGE

SP042-1 = 0.946 \Rightarrow

$p_{02} = p_s = 0.946 \times 347 = 328$ kPa

NO CREDIT FOR RESULTS OBTAINED BY USE OF INAPPROPRIATE EQ

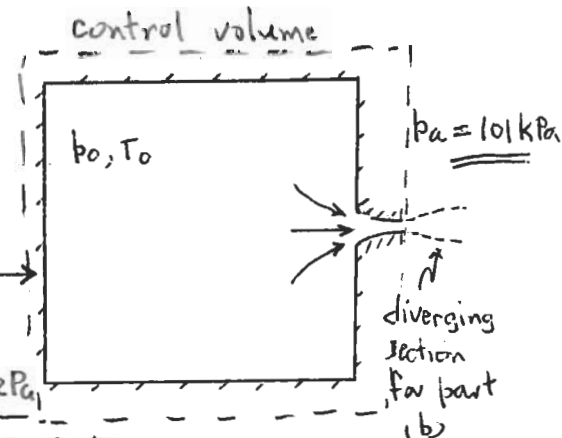
Stagnation pressure FALLS across shock

* DO NOT DO PART (C) *

IN (A) NO CREDIT UNLESS THEY TEST FOR CHOKED FLOW

MEAN
40
50 19

2. (65) The large tank contains compressed air at pressure $p_0 = 400$ kPa and temperature $T_0 = 293$ K. (Relevant properties for air are given in problem 1.) Find the horizontal component of force needed to hold the tank stationary if the air leaves to atmospheric pressure under the following conditions:



(a) through a converging nozzle with exit diameter 10 mm; and

Sonic pressure $p_* = \left(\frac{2}{\gamma+1}\right)^{\frac{\gamma}{\gamma-1}} p_0 = 0.528 p_0 = 211 \text{ kPa}$ CHECK (10)

Because $p_a = 101 \text{ kPa} < p_*$, the flow is choked and the

(35) momentum flow out of the C.V. shown is $\rho_* V_*^2 A$, CONCLUSION (10) A is exit area.

Momentum balance $F = \rho_* V_*^2 A_* + (p_* - p_a) A_* = 23.2 + 8.6 = 31.8 \text{ N}$ RESULT (5)

$\rho_* = \frac{p_0}{RT_0} \left(\frac{2}{\gamma+1}\right)^{\frac{1}{\gamma-1}} = 0.634 \frac{p_0}{RT_0} = 3.02 \text{ kg/m}^3$, $V_* = \sqrt{\frac{2}{\gamma+1} \sqrt{\gamma RT_0}} = 0.912 \sqrt{\gamma RT_0} = 313 \text{ m/s}$ (5)

(b) through a converging-diverging nozzle chosen so the exit pressure is atmospheric.

$A_* = \frac{\pi}{4} d^2 = \frac{\pi}{4} \times (10^{-2})^2 = 7.85 \times 10^{-5} \text{ m}^2$ (5)

Because the flow is choked in (a), now the momentum flow is $\rho_* V_* V_e A$

where $V_e^2 = 2\gamma p_0 \left(1 - \left(\frac{p_a}{p_0}\right)^{\frac{1}{\gamma}}\right) \Rightarrow V_e^2 = 2009 \times 293 \times \left(1 - \left(\frac{101}{400}\right)^{\frac{1}{1.4}}\right)$

$V_e = 438 \text{ m/s}$

$F = \rho_* V_* V_e A_* = 3.02 \times 313 \times 438 \times 7.85 \times 10^{-5}$

$\Rightarrow F = 32.5 \text{ N}$

$\dot{m} \quad +15$
 $V_e \quad +15$

* DO NOT DO PART (C) *

(c) For part (b), find the exit area of the nozzle.

(From $(\rho A V)^2 = (\rho_* A_* V_*)^2$,
Bernoulli eq. $\rho(p_* + \frac{1}{2} \rho V_*^2) = \rho(p_a + \frac{1}{2} \rho V_e^2)$)

NOT
GRADED

$\left(\frac{A_*}{A_e}\right)^2 = \frac{2}{\gamma-1} \left(\frac{1+\gamma}{2}\right)^{\frac{\gamma}{\gamma-1}} \left[\left(\frac{p_e}{p_0}\right)^{\frac{2}{\gamma}} - \left(\frac{p_e}{p_0}\right)^{1+\frac{1}{\gamma}} \right]$
 $= \frac{2}{.4} \left(\frac{2.4}{2}\right)^{\frac{2.4}{.4}} \left[\left(\frac{101}{400}\right)^{\frac{2}{1.4}} - \left(\frac{101}{400}\right)^{1+\frac{1}{1.4}} \right]$

$= 14.93 \times [0.1399 - 0.09447] = 0.679$

$\Rightarrow A_e = A_* / \sqrt{0.679} = 7.85 \times 10^{-5} \text{ m}^2 / 0.824 = 9.52 \times 10^{-5} \text{ m}^2$

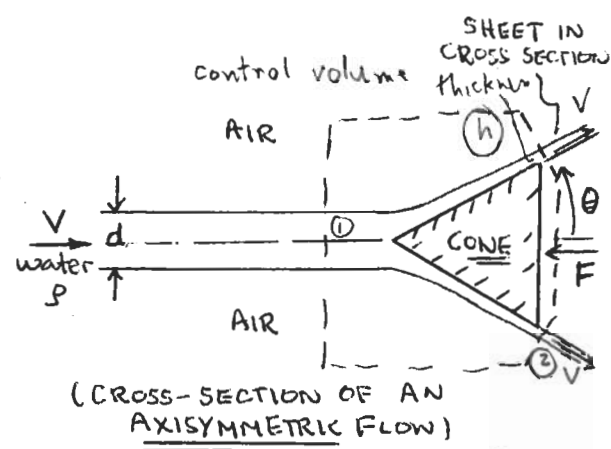
SP042-2

$\Rightarrow A_e = 9.52 \times 10^{-5} \text{ m}^2$

(d = 11 mm)

MEAN 52
SD 18

3. (70) A jet of water flows over the fixed cone and leaves as a conical sheet. The flow is incompressible and inviscid, and gravity is negligible. Using mass and momentum balances, and Bernoulli's equation, find the force F needed to hold the cone stationary in terms of the diameter d , density ρ , jet speed V and cone angle θ .



(20) By Bernoulli's equ. along the surface streamline, the speed at the exit of the CV is also V . These two points (If unif. V assumed without proof - 5)

(25) Mass balance requires mass flow rate in ① = \dot{m} = mass flow across ring ②

(25) Balance of horizontal momentum Correct momentum flows +25

$$\begin{aligned} \text{Net flow of horiz. mom. out} &= \dot{m} V \cos \theta - \dot{m} V \\ &= \text{resultant external force on all matter in CV} \\ &= -F \end{aligned}$$

$$\therefore \boxed{F = \dot{m} V (1 - \cos \theta)} \quad \left(\dot{m} = \frac{\pi}{4} \rho V^2 d^2 \right)$$

-5 Minor confusion on otherwise correct balance (eg 2 vs 3 dimensions; dimensional slips)

END

SP042-3