

Physics 7B Midterm 1

Problem 1

$$F(\vec{v}) = \frac{1}{Z} e^{-m(\vec{v}-\vec{u})^2/2kT}$$

a)1 $\langle \vec{v} \rangle = ?$ A probability distribution function for velocity v is averaged at 0 . In this case, we make a change of variable to $\vec{w} = \vec{v} - \vec{u}$. The probability distribution is then written in the more familiar way: $F(\vec{v}) = \frac{1}{Z} e^{-m\vec{w}^2/2kT}$

Since $\vec{w} = \vec{v} - \vec{u}$, the velocity average is now shifted by \vec{u} . Therefore $\langle \vec{v} \rangle = \vec{u}$.

a)2 $\langle v^2 \rangle$ From the textbook, we have $\langle v^2 \rangle = \frac{2}{m} (3/2) kT$. But since we have velocity $= \vec{w} = \vec{v} - \vec{u}$, we have

$$\langle v^2 \rangle = \frac{3}{m} kT + \vec{u}^2$$

a)3 $v_{rms} = ?$ From the textbook, we have

$$v_{rms} = \sqrt{\langle v^2 \rangle}$$

Plugging in, we have

$$v_{rms} = \sqrt{\left(\frac{3}{m} kT\right) + \vec{u}^2}$$

b) $F(v)$ is maximized when $\vec{v} = \vec{u}$:

$$F(\vec{v}) = \frac{1}{Z} e^{-m(0)^2/2kT} = \frac{1}{Z}$$

peak velocity: $\vec{v} = \vec{u}$

Note:

To see why $\langle v^2 \rangle = \frac{3kT}{m} + u^2$ we note that for $\vec{w} = \vec{v} - \vec{u}$ the distribution is the standard Maxwell distribution so

$$\langle w^2 \rangle = \frac{3kT}{m}$$

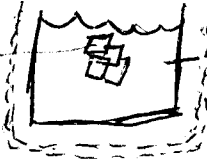
but

$$\begin{aligned}\langle w^2 \rangle &= \langle (\vec{v} - \vec{u})^2 \rangle = \langle v^2 \rangle - 2\langle \vec{u} \cdot \vec{v} \rangle + \langle u^2 \rangle \\ &= \langle v^2 \rangle - 2\vec{u} \cdot \langle \vec{v} \rangle + u^2\end{aligned}$$

Since $\langle \vec{v} \rangle = \vec{u}$, this gives

$$\langle w^2 \rangle = \langle v^2 \rangle - u^2 = \frac{3kT}{m}$$

$$\Rightarrow \langle v^2 \rangle = \frac{3kT}{m} + u^2$$

#2) a)  $\Delta Q = 0$

$$\Delta Q_{\text{ice melt}} + \Delta Q_{\text{water cool}} + \Delta Q_{\text{ice water heat}} = 0$$

* the ice will melt & then heat up from 0°C to 6°C
 * the water will cool from 49°C to 6°C

$$(0.1 \text{ kg}) L_{\text{fusion}} + (0.2 \text{ kg}) c_{\text{H}_2\text{O}} (6^\circ\text{C} - 49^\circ\text{C}) + (0.1 \text{ kg}) c_{\text{H}_2\text{O}} (6^\circ\text{C} - 0^\circ\text{C}) = 0$$

$$\Rightarrow L_{\text{fusion}} + 2 \left(1 \frac{\text{J}}{\text{K}\cdot\text{kg}} \right) (-43 \text{ K}) + 1 \left(1 \frac{\text{J}}{\text{K}\cdot\text{kg}} \right) (6 \text{ K}) = 0$$

$$L_{\text{fusion}} = 86 \text{ J} - 6 \text{ J} = \boxed{80 \text{ J/kg}}$$

b) $\Delta S = \Delta S_{\text{I}} + \Delta S_{\text{II}} + \Delta S_{\text{III}}$

$$\Delta S_{\text{I}} = \frac{m_{\text{ice}} L_{\text{fusion}}}{T} = \frac{(0.1 \text{ kg})(80 \text{ J/kg})}{273 \text{ K}} \approx \boxed{0.029 \frac{\text{J}}{\text{K}}}$$

$$\Delta S_{\text{II}} = m_{\text{H}_2\text{O}} c \int_{273}^{279} \frac{dT}{T} = (0.1 \text{ kg}) \left(1 \frac{\text{J}}{\text{K}\cdot\text{kg}} \right) \ln\left(\frac{279}{273}\right) = \boxed{0.00217 \frac{\text{J}}{\text{K}}}$$

$$\Delta S_{\text{III}} = m_{\text{H}_2\text{O}} c \int_{322}^{279} \frac{dT}{T} = (0.2 \text{ kg}) \left(1 \frac{\text{J}}{\text{K}\cdot\text{kg}} \right) \ln\left(\frac{279}{322}\right) = \boxed{-0.0286 \frac{\text{J}}{\text{K}}}$$

$$\Delta S = 0.029 \frac{\text{J}}{\text{K}} + 0.00217 \frac{\text{J}}{\text{K}} - 0.0286 \frac{\text{J}}{\text{K}} = \boxed{0.00257 \frac{\text{J}}{\text{K}}}$$

total ΔS

* 3 processes are happening

I → the ice melts in the water

II → the newly made water is heated

III → the original water is cooled

Question Three

$$W_{\text{isothermal}} = P_0 V_0 \ln\left(\frac{V_f}{V_0}\right)$$

$$W_{\text{isochoric}} = 0$$

$$P_0 = \frac{NK T_0}{V_0}$$

$$Q_{\text{isothermal}} = P_0 V_0 \ln\left(\frac{V_f}{V_0}\right)$$

$$Q_{\text{isochoric}} = \frac{d}{2} V_0 (P_f - P_0)$$

diatomic $\rightarrow d=5$

Plug in the above equations for each point on the graph,

$$\text{I) } P_1 = \frac{NK T_1}{V_1} \quad T_1 = T_H$$

$$W_{\text{I}} = T_H NK \ln\left(\frac{V_2}{V_1}\right)$$

$$Q_{\text{I}} = W_{\text{I}}$$

$$\text{II) } \Delta V = 0$$

$$W_{\text{II}} = 0$$

$$Q_{\text{II}} = \frac{5}{2} V_2 (P_3 - P_2)$$

$$Q_{\text{II}} = \frac{5}{2} NK (T_C - T_H)$$

$$\text{III) } W_{\text{III}} = NK T_C \ln\left(\frac{V_1}{V_2}\right)$$

$$W_{\text{III}} = Q_{\text{III}}$$

$$\text{IV) } W_{\text{IV}} = 0$$

$$Q_{\text{IV}} = \frac{5}{2} NK (T_H - T_C)$$

note : $NK = nR$

$$T_1 = T_{II} = T_H$$

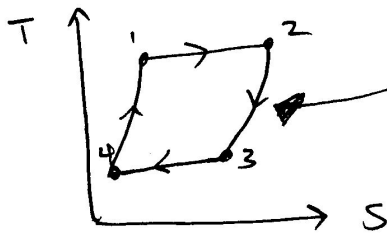
$$T_{III} = T_{IV} = T_C$$

$$V_1 = V_{IV}$$

$$V_{II} = V_{III}$$

Question Three

b) This is a Stirling engine



The isochoric legs go
as the log

for the isochoric sections

$$dQ = \frac{5}{2} Nk dT$$

$$\int ds = \int \frac{dQ}{T} = \frac{5}{2} Nk \int \frac{dT}{T} = \frac{5}{2} Nk \ln(T) + \text{const.}$$

$$c) e = \frac{W}{Q_H} = \frac{W_I + W_{III}}{Q_I + Q_{IV}}$$

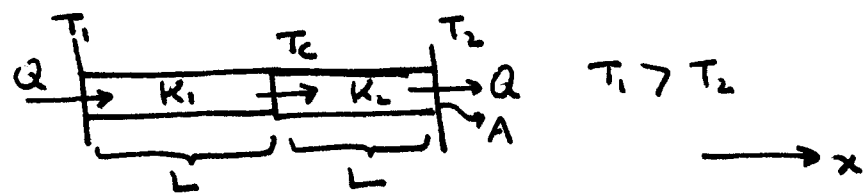
$$= \frac{Nk \ln(v_2/v_1) (T_H - T_C)}{T_H Nk \ln(v_2/v_1) + \frac{5}{2} Nk (T_H - T_C)} \times 100\%$$

$$= \frac{\ln(5) (400 - 300)}{400 \ln(5) + \frac{5}{2} (400 - 300)} \times 100\%$$

$$e = 18\%$$

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(a) SERIES:



In steady state, Temperature only depends on location x not time
 • Heat flow $\frac{dQ}{dt}$ constant throughout.

$$\frac{dQ}{dt} = \text{CONST} = \frac{K_1 A (T_1 - T_c)}{L} = \frac{K_2 A (T_c - T_2)}{L}$$

$$\Rightarrow K_1 T_1 - K_1 T_c = K_2 T_c - K_2 T_2 \Rightarrow T_c = \frac{K_1 \cdot T_1 + K_2 \cdot T_2}{K_1 + K_2}$$

Temp. at the interface

Plug T_c into $\frac{dQ}{dt}$ above, say 1st one:

$$\frac{dQ}{dt} = \frac{K_1 A}{L} \left(T_1 - \frac{K_1 T_1 + K_2 T_2}{K_1 + K_2} \right) = \frac{K_1 A}{L} \left(\frac{K_1 T_1 + K_2 T_1 - K_1 T_1 - K_2 T_2}{K_1 + K_2} \right) = \frac{K_1 A}{L} \frac{K_2 (T_1 - T_2)}{K_1 + K_2}$$

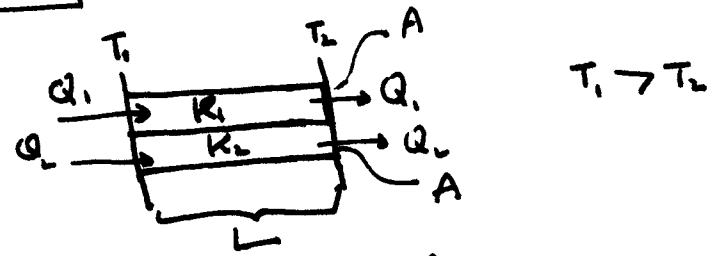
$$\Rightarrow \frac{dQ}{dt} = \frac{K_1 K_2 \cdot A}{K_1 + K_2} \frac{(T_1 - T_2)}{L} = \frac{2 K_1 K_2}{K_1 + K_2} \cdot \frac{A}{2L} (T_1 - T_2)$$

$$\frac{dQ}{dt} = \frac{2 K_1 K_2 \cdot A}{K_1 + K_2} \frac{(T_1 - T_2)}{2L}$$

$\equiv K_{eff}$ single rod with length $2L$, cross section

$$\Rightarrow K_{eff} = \frac{2 K_1 K_2}{K_1 + K_2} \quad \text{check: } K_1 = K_2 \Rightarrow K_{eff} = K \checkmark$$

(b) Parallel:



In steady state heat flow through each constant

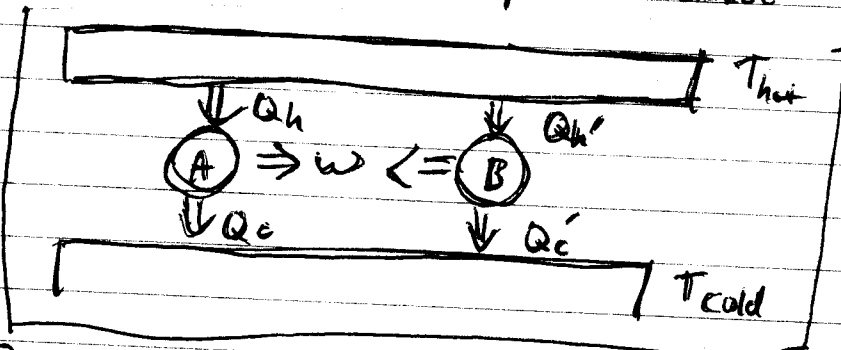
$$\frac{dQ}{dt} = \frac{dQ_1}{dt} + \frac{dQ_2}{dt} = K_1 \frac{A}{L} (T_1 - T_2) + K_2 \frac{A}{L} (T_1 - T_2)$$

$$\frac{dQ}{dt} = (K_1 + K_2) \frac{A}{L} (T_1 - T_2) \Rightarrow \frac{dQ}{dt} = \left(\frac{K_1 + K_2}{2} \right) \frac{2A}{L} (T_1 - T_2)$$

$$K_{eff} = \frac{K_1 + K_2}{2} \quad \text{check: } K_1 = K_2 \Rightarrow K_{eff} = K \checkmark \quad \equiv K_{eff} \quad \text{single rod of } 2A \text{ and } L$$

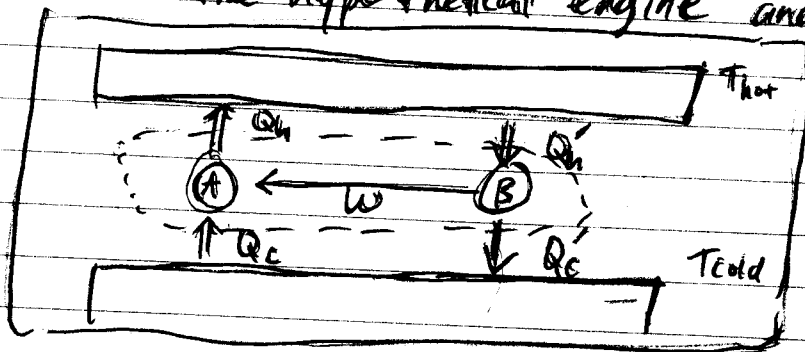
Suppose there exists a hypothetical engine ^(B) with greater efficiency than a Carnot Engine (A)

We adjust the cycle of the Carnot engine such that its work output $w_{\text{Carnot}} = w_{\text{hypothetical}} = w$.



This means
 $Q'_h - Q'_c = w$
 $Q_h - Q_c = w$

Since the Carnot engine is reversible, we can turn it into a refrigerator that takes in work w from the hypothetical engine and energy Q_c from the cold reservoir



and the outputs energy Q_h into the hot reservoir.

Let's look at what this means ^{so} also

$$\frac{w}{Q'_h} > \frac{w}{Q_h} \Rightarrow Q_h > Q'_h$$

$$\left. \begin{array}{l} Q_c + w = Q_h \\ -Q'_c - w = -Q'_h \end{array} \right\} \Rightarrow Q_c - Q'_c = Q_h - Q'_h > 0$$

Look at the net effect of the 2-engine contraption we made. It takes a positive amount of heat $(Q_c - Q'_c)$ from the cold reservoir & moves it to the hot reservoir with no work! This violates the 2nd law!

this cannot be!