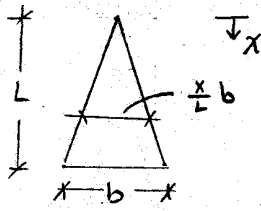


Prob 1



$$\text{Axial force: } P_x = \gamma \left(\frac{1}{2} \cdot x \cdot \frac{x}{L} b \cdot L \right) = \frac{1}{2} \frac{b\gamma}{L} x^2$$

$$\text{Cross-section: } A_x = \left(\frac{x}{L} b \right) \cdot L = \frac{b}{L} x$$

$$\Delta = \int_0^L \frac{P_x dx}{A_x E} = \int_0^L \frac{\frac{1}{2} \frac{b\gamma}{L} x^2 dx}{\frac{b}{L} \cdot x E} = \frac{\gamma}{2E} \int_0^L x dx = \boxed{\frac{\gamma L^2}{4E}}$$

Prob 2

Stresses

$$\begin{array}{lll} P_x = 40 \text{ Kips} & A_x = 2.4 & \sigma_x = 5 \text{ Ksi} \\ P_y = 48 \text{ Kips} & A_y = 2.3 & \sigma_y = 8 \text{ Ksi} \\ P_z = 36 \text{ Kips} & A_z = 3.4 & \sigma_z = 3 \text{ Ksi} \end{array}$$

E

$$E = 2(1+\nu)G = 2(1+0.25)4 \times 10^6 = 10 \times 10^6 \text{ psi} = 10 \times 10^3 \text{ Ksi}$$

 ϵ_x

$$\epsilon_x = \frac{1}{E} (\sigma_x - \nu \sigma_y - \nu \sigma_z) = \frac{1}{E} [5 - 0.25(8+3)] = 2.25 \times 10^{-4}$$

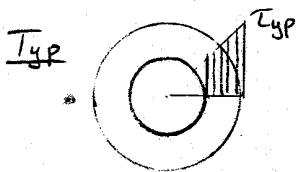
 P_x'

$$\epsilon_x = \epsilon_x' = \frac{\sigma_x'}{E} \quad P_x' = \sigma_x' A_x$$

$$\sigma_x' = E \cdot \epsilon_x = (10 \times 10^3 \text{ Ksi})(2.25 \times 10^{-4}) = 2.25 \text{ Ksi}$$

$$P_x' = 2.25 \text{ Ksi} (2.4) = \boxed{18 \text{ Kips}}$$

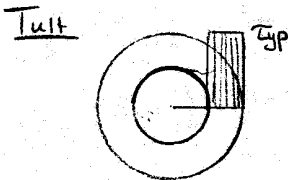
Prob 3



$$T_{yp} = \frac{\tau_{yp} I_p}{c}$$

$$I_p = \frac{\pi}{2} \left(c^4 - \left(\frac{c}{2} \right)^4 \right) = \frac{15}{32} \pi c^4$$

$$T_{yp} = \frac{15}{32} \tau_{yp} c^3 \pi$$



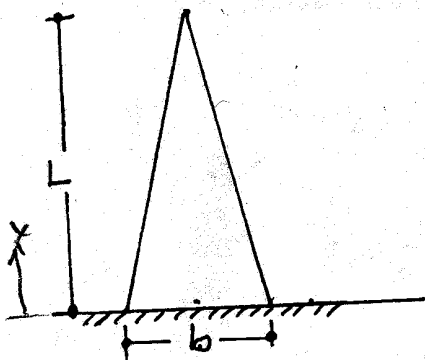
$$T = \int \tau 2\pi p^2 dp$$

$$T_{yt} = \int_{c/2}^c \tau_{yp} 2\pi p^2 dp = 2\pi \tau_{yp} \left. \frac{1}{3} p^3 \right|_{c/2}^c$$

$$= 2\pi \tau_{yp} \frac{1}{3} \left(c^3 - \frac{c^3}{8} \right) = \frac{7}{12} \tau_{yp} \pi c^3$$

$$\frac{T_{yt}}{T_{yp}} = \frac{\frac{7}{12} \tau_{yp} \pi c^3}{\frac{15}{32} \tau_{yp} \pi c^3} = \frac{7}{12} \cdot \frac{32}{15} = \frac{56}{45} = \boxed{1.24}$$

1. The triangular bar shown is cut from a 1-in. thick plate. Determine the deflection of the top due to the weight of the bar. The unit weight of the material is γ ; the elastic modulus is E . (Obvious assumption: Bar does not fall over)



$$m = \gamma t \frac{1}{2} wh$$

$$w = \frac{(L-x)b}{L}$$

$$h = (L-x)$$

$$P = w = \gamma t \frac{1}{2} \left(\frac{L-x}{L}\right) b (L-x)$$

$$A = tw = t \left(\frac{L-x}{L}\right) b$$

$$\Delta = \int_0^L \frac{P}{AE} dx = \frac{1}{E} \int_0^L \frac{P}{A} dx$$

$$= \frac{1}{E} \int_0^L \frac{\frac{1}{2} \gamma t \left(\frac{L-x}{L}\right) b (L-x)}{t \left(\frac{L-x}{L}\right) b} dx$$

$$= \frac{1}{E} \int_0^L \frac{\gamma (L-x)}{2} dx$$

$$= \frac{\gamma}{2E} \int_0^L (L-x) dx$$

$$= \frac{\gamma}{2E} \left[Lx - \frac{x^2}{2} \right]_0^L$$

$$= \frac{\gamma}{2E} \left[L^2 - \frac{L^2}{2} \right]$$

$$= \frac{\gamma}{2E} \left[\frac{L^2}{2} \right]$$

$$\Delta = \frac{\gamma L^2}{4E} \text{ downward}$$

Good!

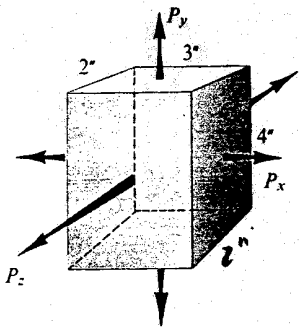
$$P = w = \gamma V = \gamma t SA = \gamma t \frac{1}{2} \text{ base} \cdot \text{height}$$

$$\text{base} = \left(\frac{L-x}{L}\right) b \quad \text{height} = L-x$$

$$P = \frac{1}{2} \gamma t \left(\frac{L-x}{L}\right) b (L-x)$$

Tom Allen

2. A rectangular aluminum alloy block has the dimensions shown in the figure. The resultants of uniformly distributed stresses are $P_x = 40$ kips, $P_y = 48$ kips, and $P_z = 36$ kips. Determine the magnitude of a single system of tensile forces acting only in the x direction which would cause the same deformation in the x direction as the initial forces. Let $G = 4 \times 10^6$ psi, and $\nu = 0.25$.



$$\epsilon_x = \frac{P_x}{A_x E} - \nu \frac{P_y}{A_y E} - \nu \frac{P_z}{A_z E}$$

$$\epsilon_x = \frac{40}{2.4 \cdot 10 \times 10^3} - 0.25 \frac{48}{2.3 \cdot 10 \times 10^3} - \frac{36}{3.4 \cdot 10 \times 10^3}$$

$$\epsilon_x = 2.25 \times 10^{-4} \frac{\text{in}}{\text{in}}$$

$$E = 2G(1 + \nu)$$

$$= 2(4 \times 10^6)(1 + 0.25)$$

$$E = 10 \times 10^6 \text{ psi}$$

$$= 10 \times 10^3 \text{ ksi}$$

$$\epsilon_x = \frac{P_x}{A_x E} = 2.25 \times 10^{-4} \frac{\text{in}}{\text{in}}$$

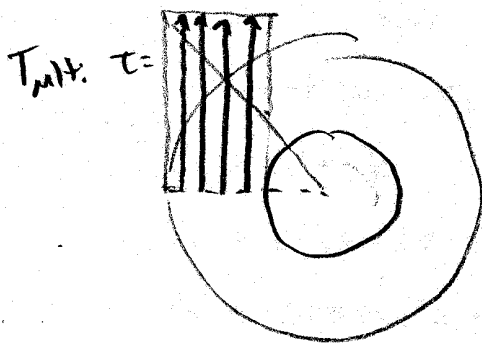
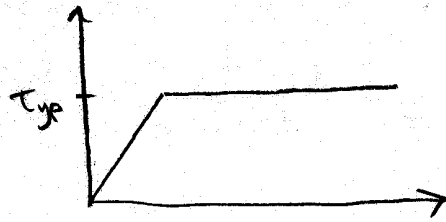
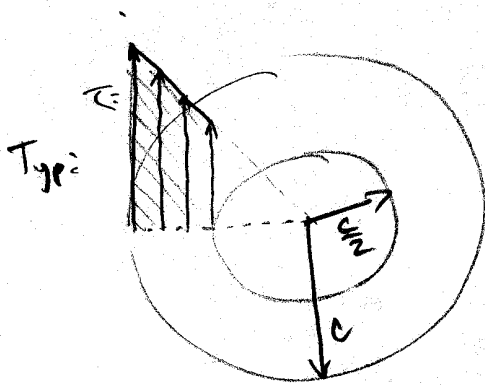
$$P_x = (2.25 \times 10^{-4})(A_x)(E)$$

$$P_x = (2.25 \times 10^{-4})(2.4)(10 \times 10^3)$$

$$P_x = 18 \text{ kips}$$

good

3. Determine the ratio of the ultimate plastic torque T_{ult} to the yield torque T_{yp} for a tubular bar of circular cross-section. The inside radius is half of the outside radius c . Assume that the bar is made of an elastoplastic material.



$$T = \int \tau p dA$$

$$\text{for } y_p \quad \tau = \tau_{yp} \frac{p}{c}$$

$$T = \int \tau_{yp} \frac{p}{c} \cdot p dA$$

$$= \int_{\frac{c}{2}}^c \tau_{yp} \cdot \frac{p}{c} \cdot 2\pi p dp$$

$$= \int_{\frac{c}{2}}^c \tau_{yp} \frac{p^2}{c} \cdot 2\pi dp$$

$$= 2\pi \frac{\tau_{yp}}{c} \int_{\frac{c}{2}}^c p^3 dp = \frac{2\pi \tau_{yp}}{c} \left[\frac{p^4}{4} \right]_{\frac{c}{2}}^c$$

$$= \frac{2\pi \tau_{yp}}{c} \left[\frac{c^4}{4} - \frac{(\frac{c}{2})^4}{4} \right]$$

$$= \frac{2\pi \tau_{yp}}{c} \left[\frac{16c^4}{64} - \frac{c^4}{64} \right] = \left(\frac{2\pi \tau_{yp}}{c} \right) \left(\frac{15}{64} c^4 \right)$$

$$T_{yp} = \frac{30\pi \tau_{yp} c^3}{64}$$

for ultimate plastic torque
 $\tau = \tau_{yp}$

$$T_{ult} = \int \tau_{yp} p dA =$$

$$= \tau_{yp} \int p \cdot 2\pi p dp$$

$$= 2\pi \tau_{yp} \int_{\frac{c}{2}}^c p^2 dp$$

$$= 2\pi \tau_{yp} \left[\frac{p^3}{3} \right]_{\frac{c}{2}}^c$$

$$= 2\pi \tau_{yp} \left[\frac{c^3}{3} - \frac{(\frac{c}{2})^3}{3} \right]$$

$$= 2\pi \tau_{yp} \left[\frac{8c^3}{24} - \frac{c^3}{24} \right]$$

$$= 2\pi \tau_{yp} \left(\frac{7c^3}{24} \right)$$

$$T_{ult} = \frac{14\pi \tau_{yp} c^3}{24}$$

$$\frac{T_{ult}}{T_{yp}} = \frac{\frac{14\pi \tau_{yp} c^3}{24}}{\frac{30\pi \tau_{yp} c^3}{64}} = \frac{14 \cdot 64}{30 \cdot 24} = \frac{56}{45} = \boxed{1.244}$$

great